

# Low Temperature Co-fired Ceramic

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# Outline

- **What is LTCC?**
- **Advantages**
- **Process of LTCC**
- **Applications of LTCC**
- **Future developments**
- **Case study**
- **Conclusion**

# What is LTCC? (1/1)



- Multilayer
- Size and cost reduction for many applications
- Frequency range from 100 MHz to 40 GHz
- Use of buried components: resistors, capacitors, and inductors
- High density of interconnections with three-dimensional design

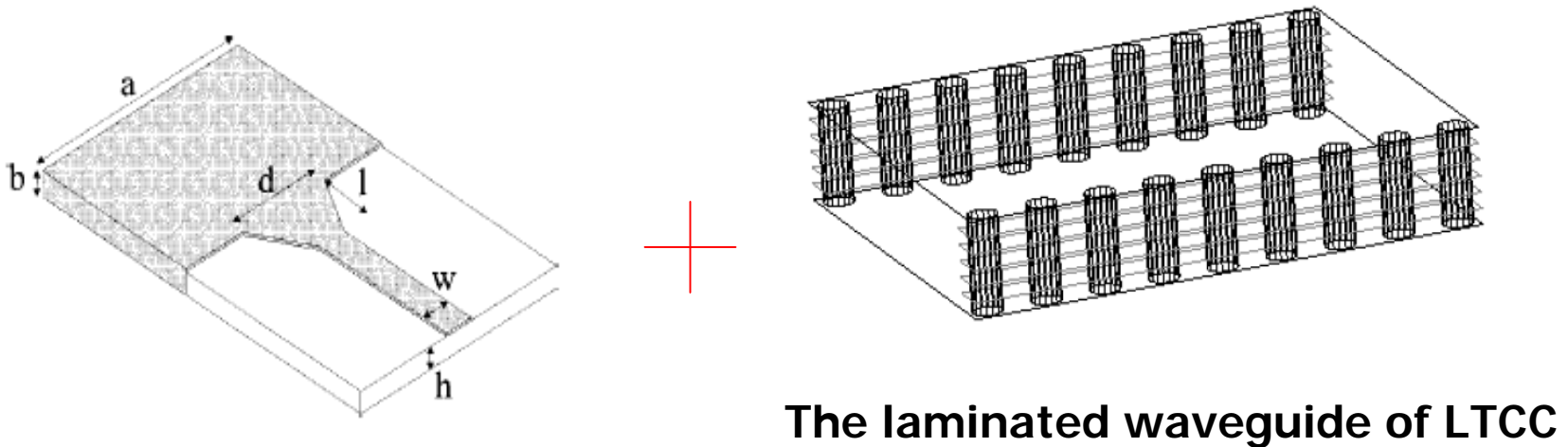


# What is LTCC? (2/2)

- Optimized transitions (from planar circuitry to rectangular <or circular> waveguides. )
- Packaging solutions
- Thermal management for heat dissipation in power applications
- In-house LTCC prototype manufacturing design and characterization of modules and antennas

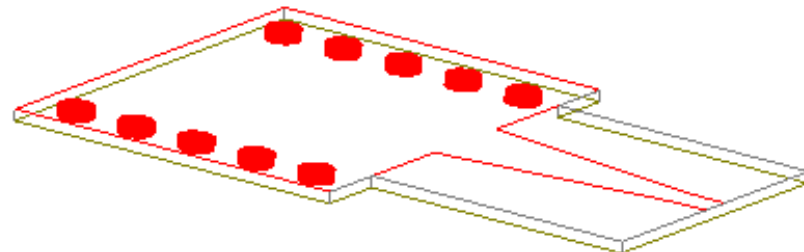
# LTCC Transition

The transition between microstrip line and the laminated waveguide of LTCC

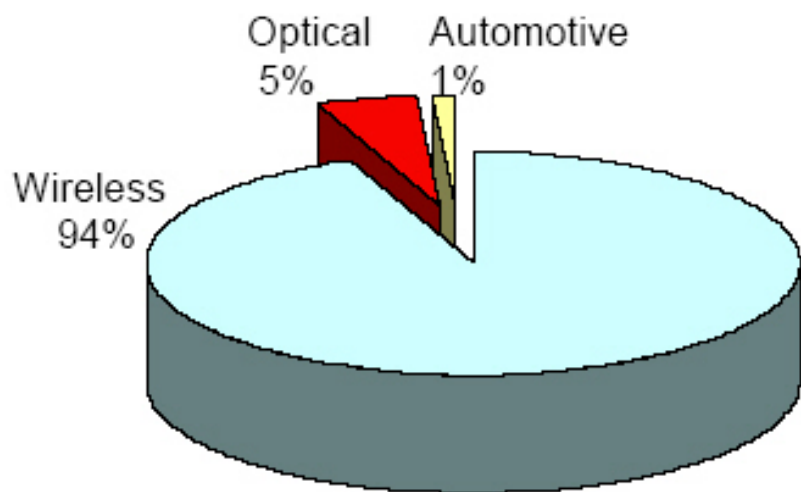


The laminated waveguide of LTCC

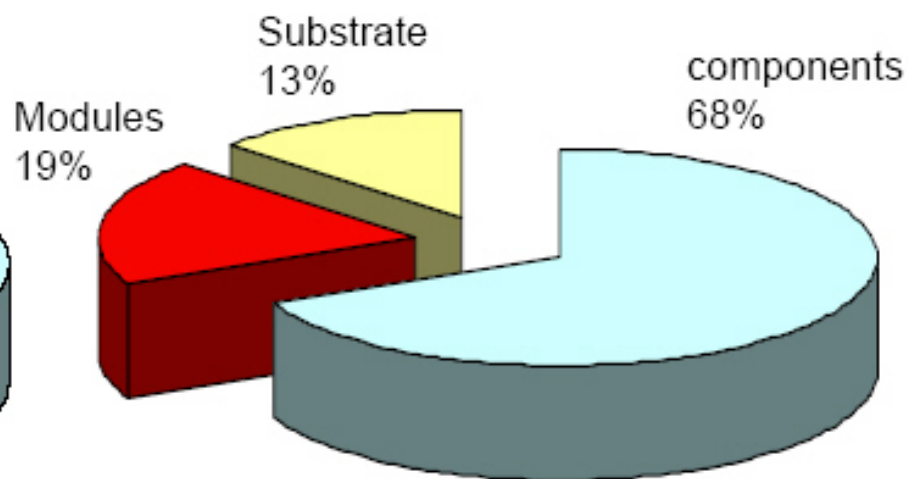
Fig. 1. Configuration of the proposed transition of microstrip line to rectangular waveguide on the same substrate.



# LTCC product market

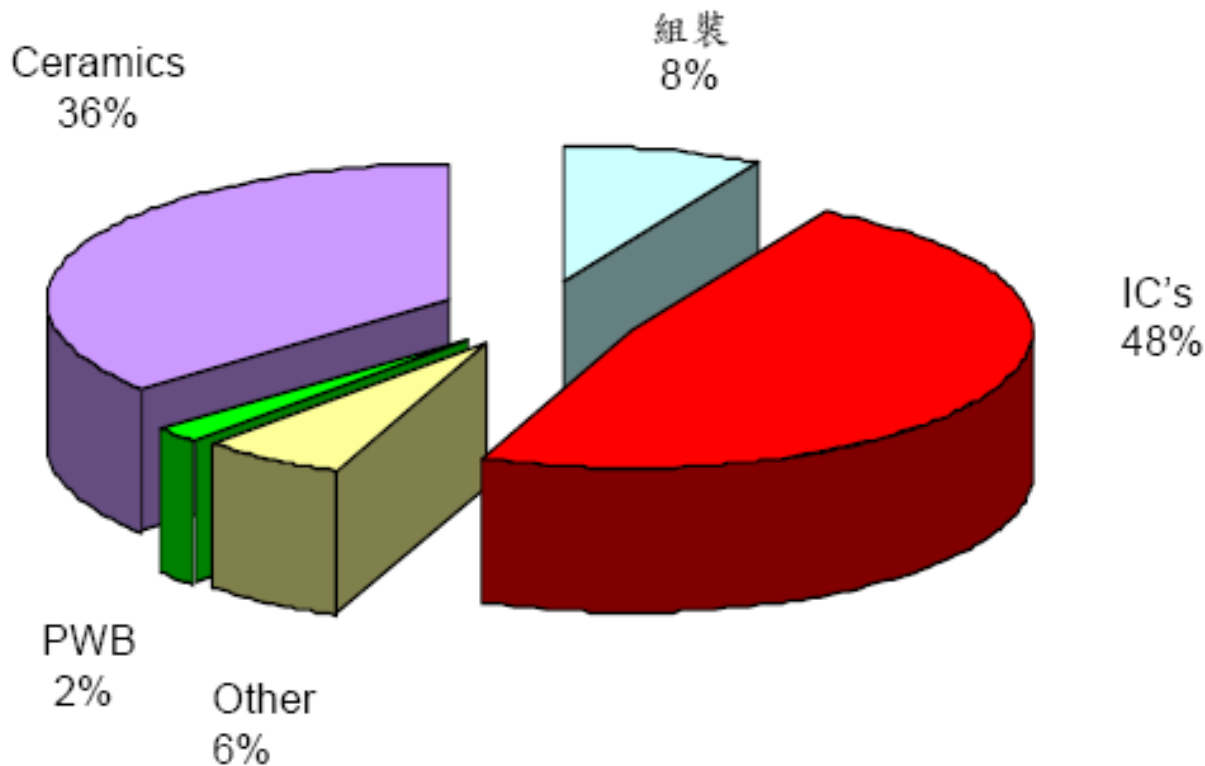


用途數量規模



分類數量規模

# Cost Distribution for Typical Wireless Transceiver



PWB (Printed Wiring Board)

Source: 1997 MCM Conference



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# Difference between HTCC and LTCC

	LTCC	HTCC
Co-fired temperature	850°C	1950°C
metal	a lower fusion point metal	a higher fusion point metal
Quality	High	low

# Why use LTCC?

	LTCC	HTCC	Organic
Conductor Material	Cu or Ag	W or Mo	Cu
Conductor loss	1	3	1
Dielectric loss	2	1	3
Total loss	1	2	3
CTE compared to Si	1	2	3
Thermal conductivity	2	1	3
Embedded passive components	1	3	2
Layer number	1	3	2
Miniaturization for passive components	1	2	2
Miniaturization for active components	2	3	1

1最佳 2普通 3較差

CTE : Co-efficient of Thermal Expansion



# Conductor Properties

Material	Resistivity( $m\Omega/cm$ )	Melting Point( $^{\circ}C$ )
Silver (Ag)	1.63	961
Copper (Cu)	1.72	1083
Gold (Au)	2.44	1063
Wolfram (W)	5.51	3370

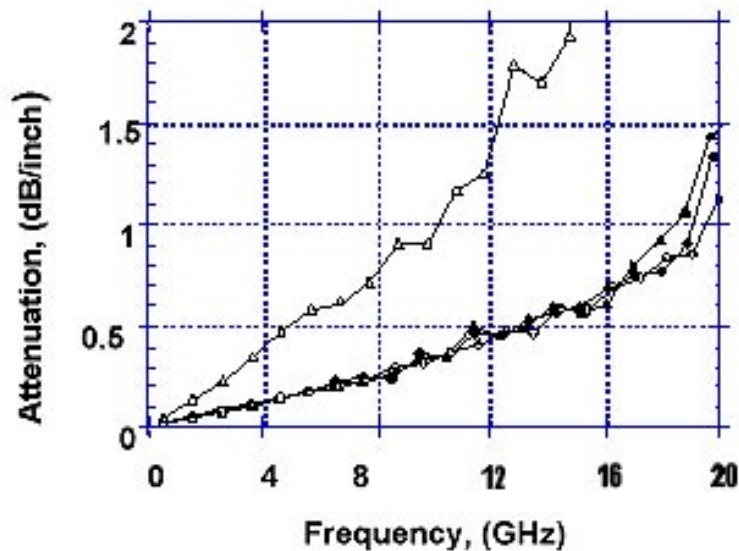
# Material Properties

Tape Type	Dupont 951	Dupont 943
Dielectric constant @ 1MHz	7.8	7.4
Loss tangent @ 1MHz	0.0015	0.0009
Shrinkage (X, Y)	~13%	~10.3%
Shrinkage (Z)	~15%	~14.5%
TCE (ppm/°C)	5.8	6.0
Thermal Conductivity (W/m °K)	3.0	4.4
Tape Thickness (mils)	1.7, 3.7, 5.3...	4.27...

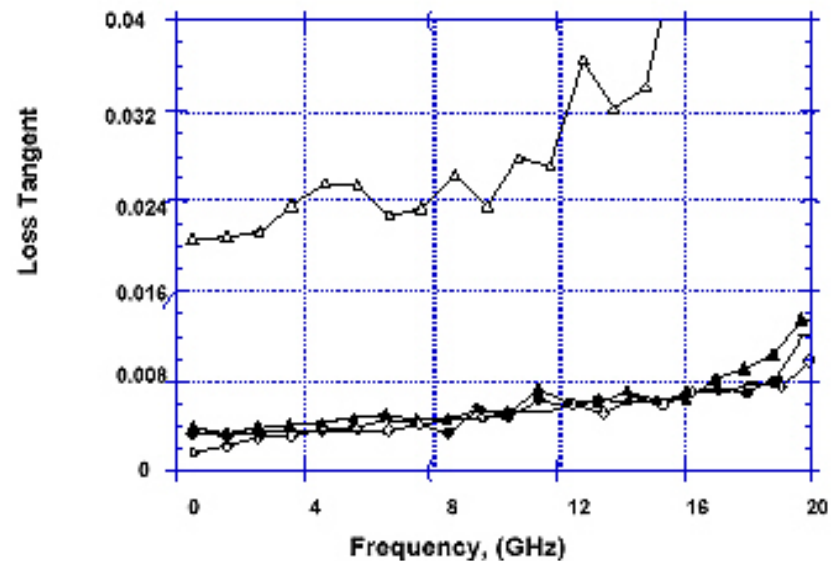
TCE : Temperature Coefficient of Expansion

# High Frequency Characterization

- ◆ 951 Green Tape™/5734 Gold Conductor
- ▲ 951 Green Tape™/6142 Silver Conductor
- ◇ 951 Green Tape™/Fodel® Silver Conductor
- ▽ FR4 PWB/Unplated Copper Conductor



- 951 Green Tape™ / 5734 Gold Conductor
- ▲ 951 Green Tape™ / 6142 Silver Conductor
- ◇ 951 Green Tape™ / Fodel® Silver Conductor
- △ FR4 PWB / Unplated Copper Conductor



# Benefits ( 1 / 3 )

- Integrated passives --- reliability, size reduction
- High Q, low loss
- Outstanding reliability
- 3-D design
- Controlled impedance(內部接線的阻抗)
- Environmental stability(熱膨脹係數低)



# Benefits ( 2 / 3 )

- Direct chip attach---TCE matching to Si and GaAs
- Rapid prototyping
- Volume manufacturing capacity
- every single layer can be inspected (and in the case of inaccuracy or damage) replaced before firing; this prevents the need of manufacturing a whole new circuit.



# Benefits ( 3 / 3 )

- integrating components is Cost reduction
- A clear advantage over other multichip module (MCM) technologies in integrating passive components

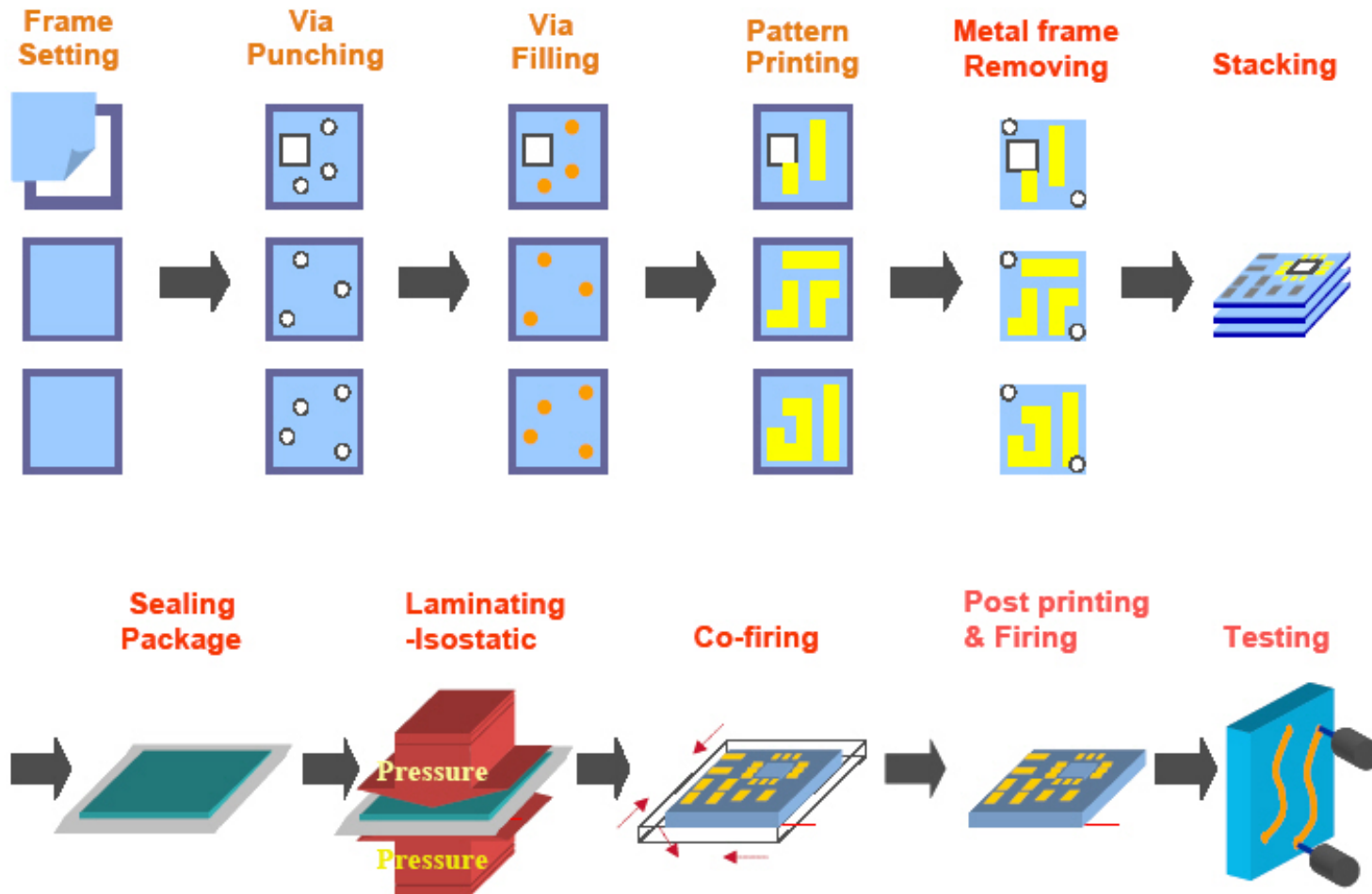




# Outline

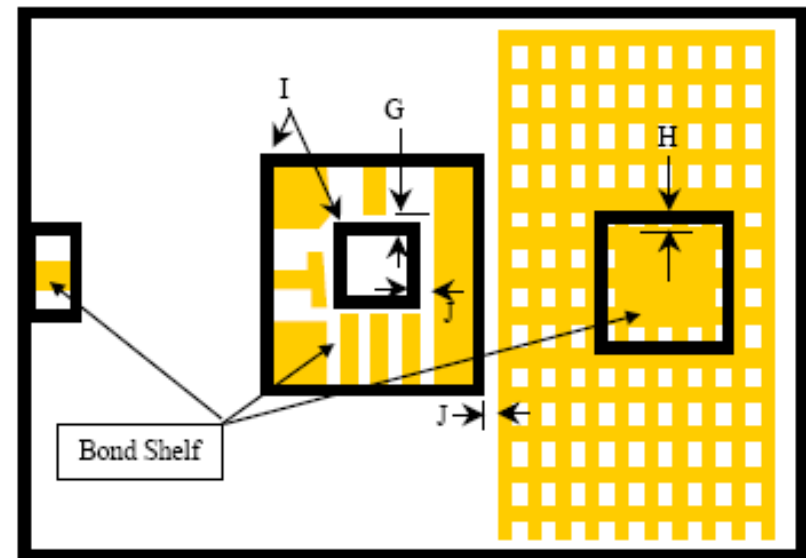
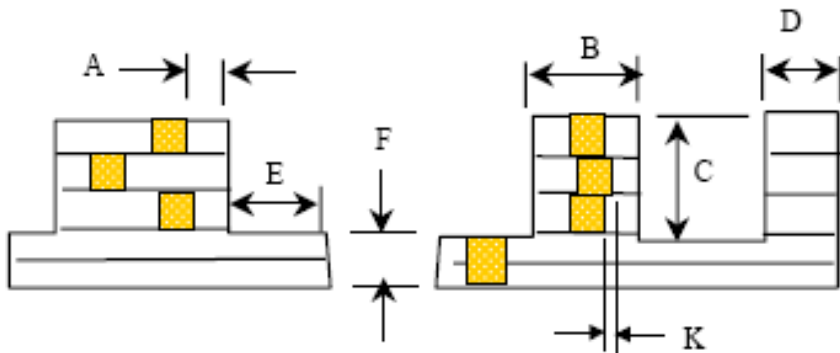
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# Process of LTCC



# CAVITIES

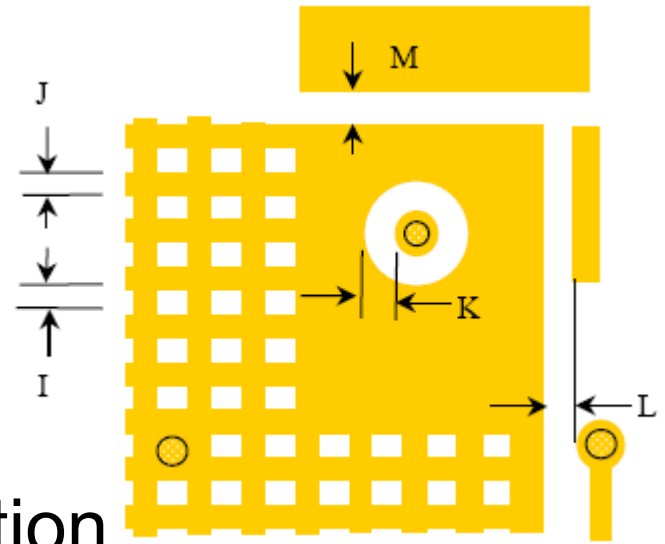
- Cavity design is complicated by concerns of deformation during lamination and firing, particularly of thin or deep walls.



# GROUND PLANES

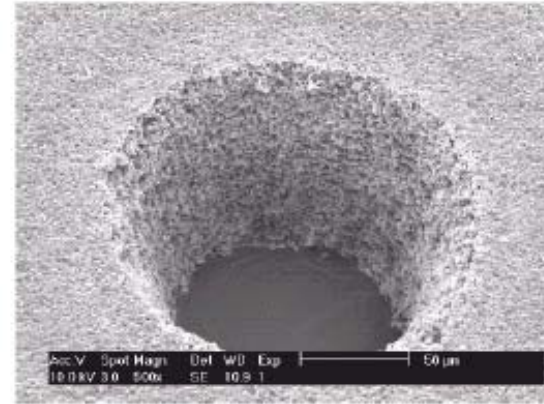
- Gridded ground planes

- use less precious metal
- create less ceramic distortion
- Lines half as wide as spaces result in 55% metal coverage, and are recommended.
- Solid areas are required at via landings and may be added at other locations.

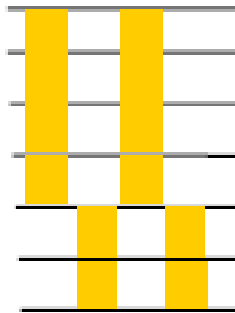


# Three general types of Vias(1/3)

- RF shield vias –
  - cover pads optional

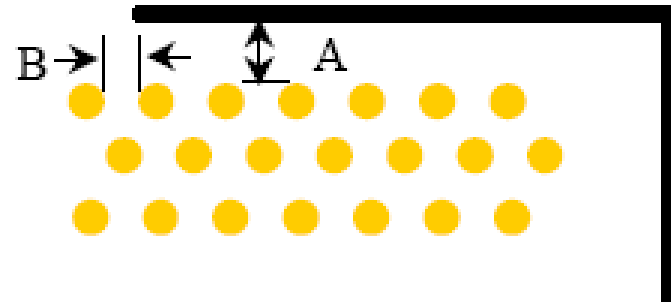


Stack offset  
for hermeticity



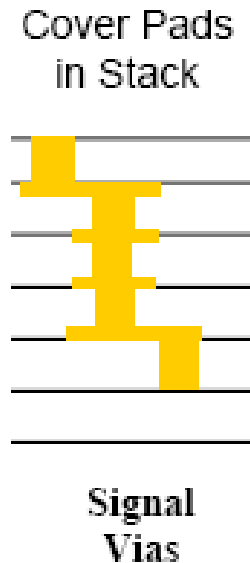
RF Shield  
Vias

RF Shield Vias

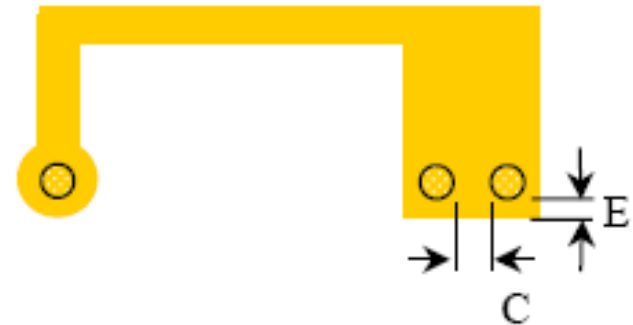


# Three general types of Vias(2/3)

- signal vias –
  - cover pads recommend



Signal Vias

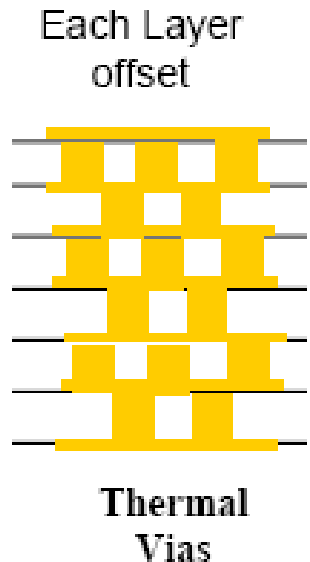


Via sizes are limited by tape thickness, due to aspect ratio of filling the vias. Keeping aspect ratio of via to tape close to 1 is optimum for manufacturability.

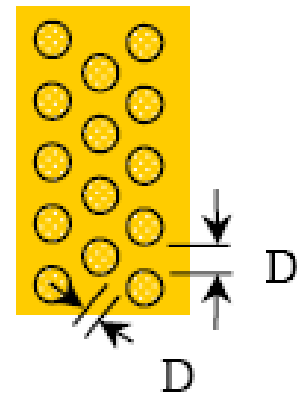
# Three general types of Vias(3/3)

- thermal vias –

- connected by planes
- staggered with planes at each layer

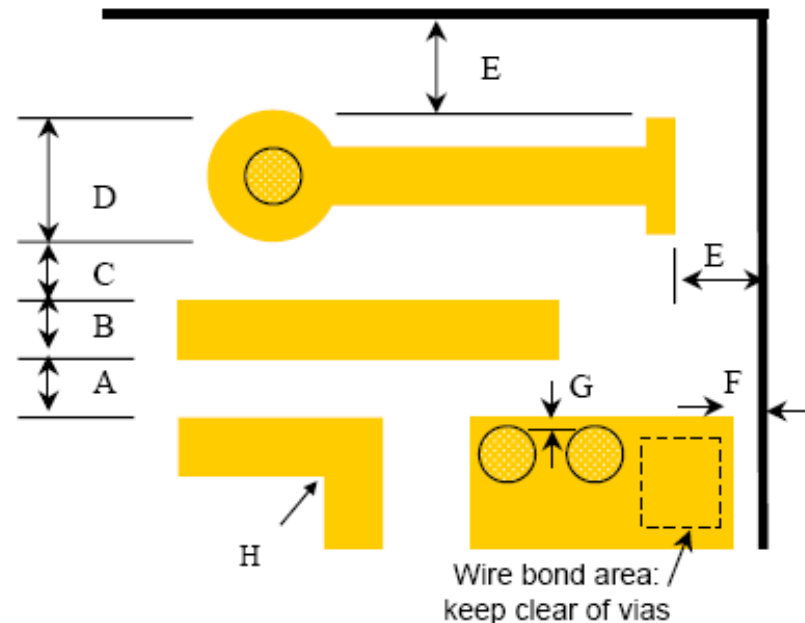
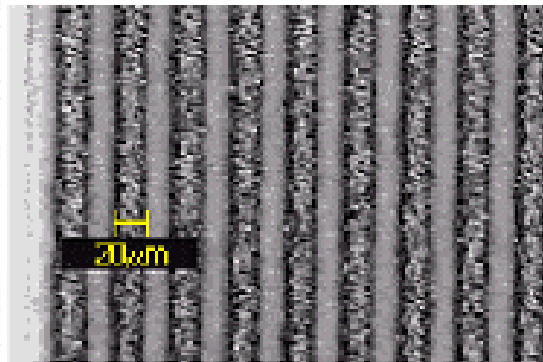


Thermal Vias



# CONDUCTORS

- Conductors are typically printed on the green tape
- Placement close to cut edges must be carefully



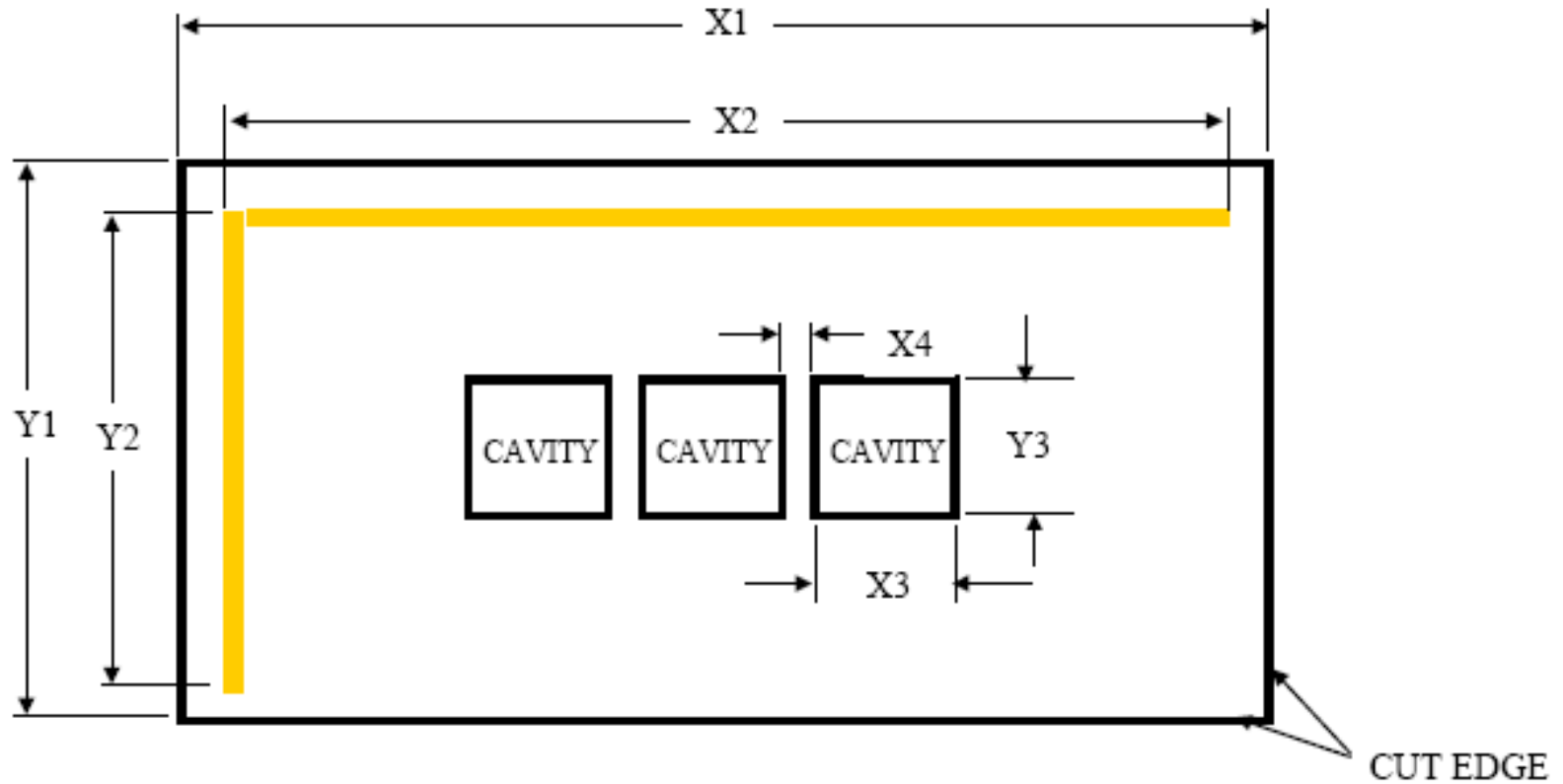




# CUTTING PROCESSES

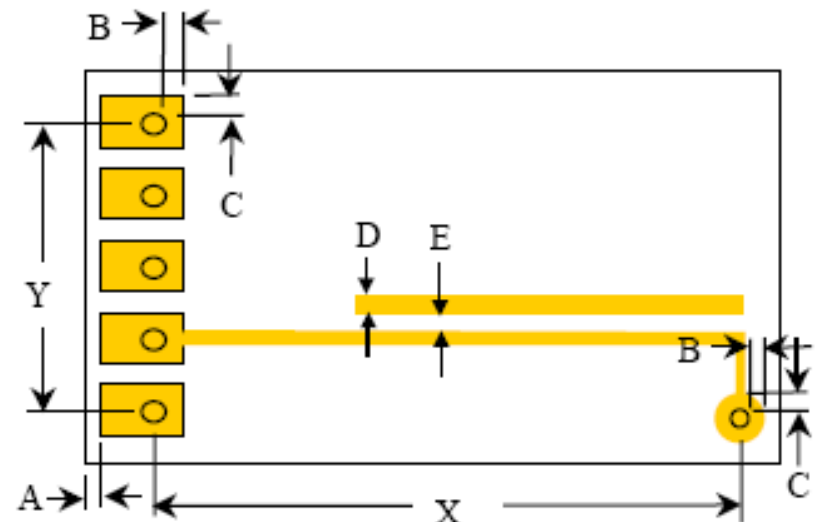
- Hot Knife
- Saw Cut
- Laser Cut
- Laser Scribe
- Hot Knife Scribe

# PACKAGE DESIGN

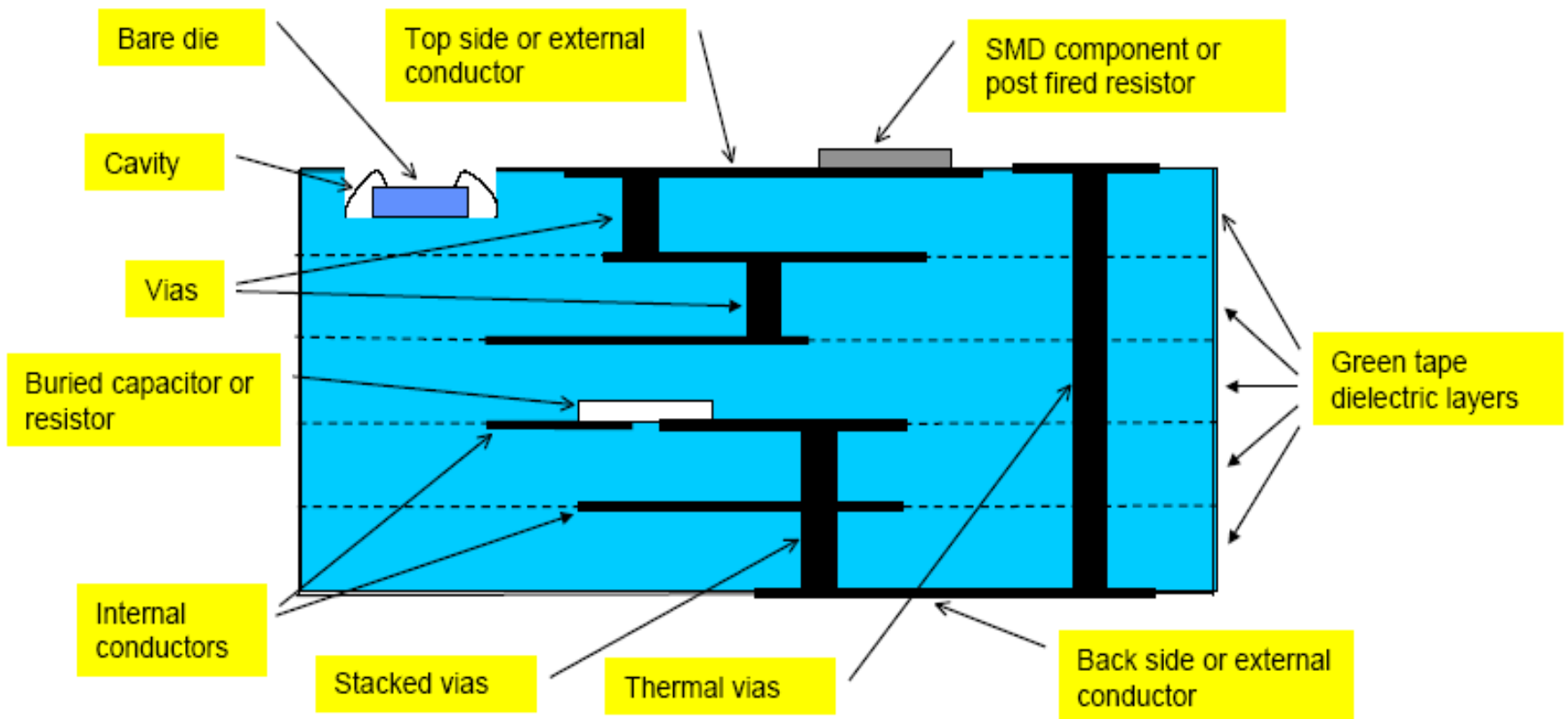


# POST PRINT

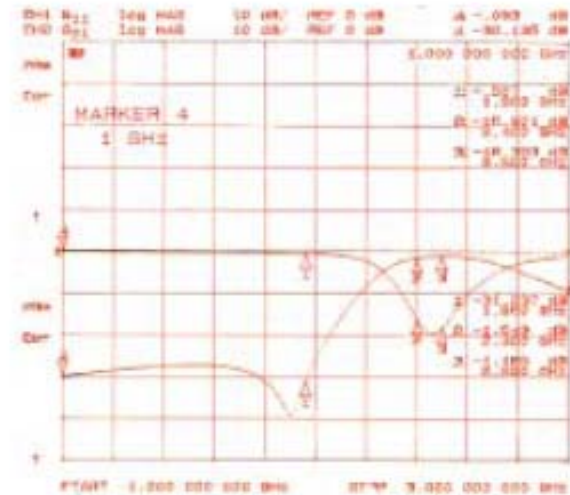
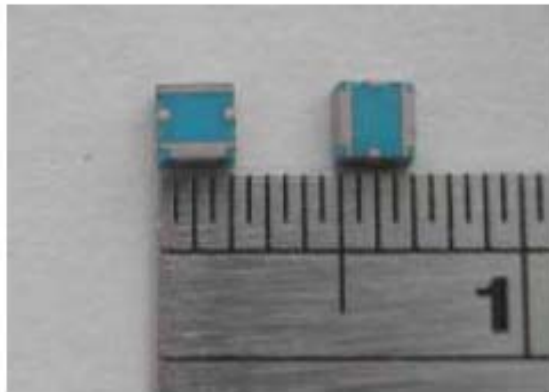
- Post printing refers to the process of printing conductors after firing the package, usually after cutting to size.
- Post printing will also be required if grinding is necessary.
- the catch pad sizes must be sufficiently large



# Cross Section of LTCC Modules

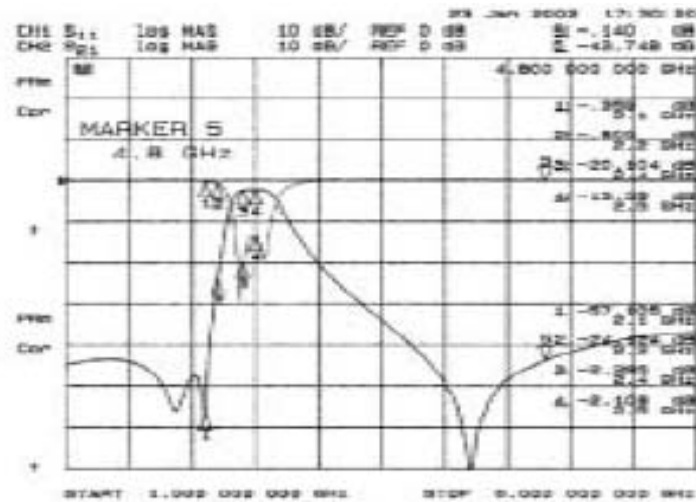
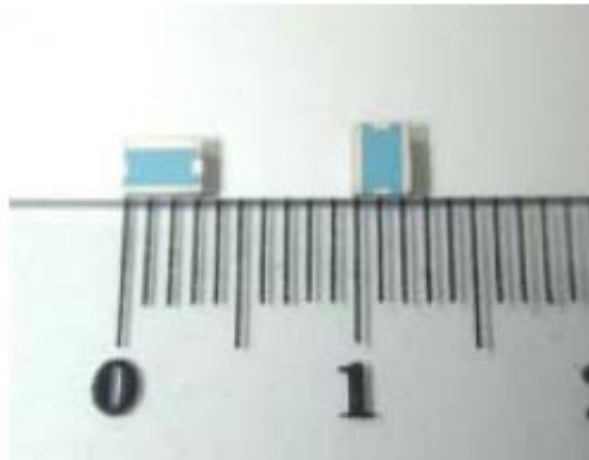


# 2.4 GHz LTCC Filter



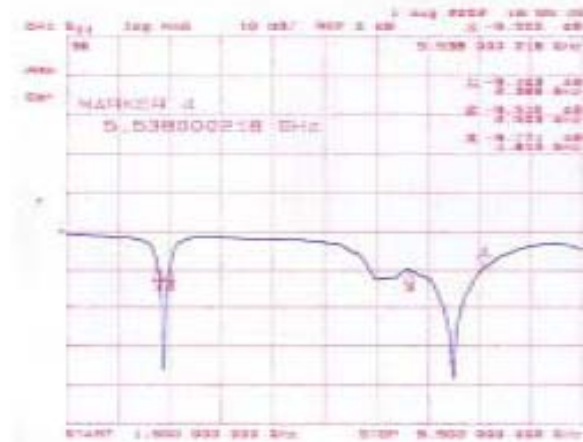
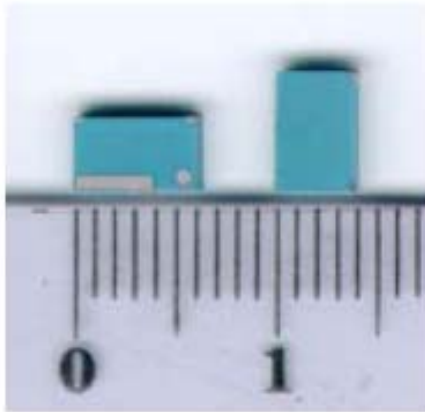
Item	Spec.
Center Freq.( $f_0$ )	2.45GHz
Bandwidth	$f_0 \pm 50\text{MHz}$
Insertion Loss	2 dB max.
Attenuation	30 dB min. @ 1.96GHz
Size( $\text{mm}^3$ )	2 x 2 x 1.5

# 2.4 GHz LTCC High-Rejection-Rate Filter



ITEM	SPECIFICATION	MEASUREMENT
Center Frequency ( $f_0$ )	2442 MHz	2442 MHz
Bandwidth (BW)	83 MHz min.	> 83 MHz
Insertion Loss @ BW	2.8 dB max.	2.5 dB max.
Ripple @ BW	1.5 dB max.	0.6 dB max.
Return Loss @ BW	10 dB min.	13 dB min.
Attenuation @ 1750-1950MHz	40 dB min.	40 dB min.
@ 2100MHz	35 dB min.	40 dB
@ 2200MHz	20 dB min.	24 dB
Size	3.2 x 2.5 x 1.7 mm <sup>3</sup>	3.2 x 2.5 x 1.46 mm <sup>3</sup>
Substrate/Package	LTCC	LTCC

# MLC/LTCC Embedded Antenna



Items	Measurement	
	ISM 2.4 GHz	ISM 5 GHz
Bandwidth	110 MHz	1100 MHz
VSWR	2.0	2.0
Gain	1.0 dBi	1.8 dBi
Polarization	Linear	Linear
Azimuth beam width	Omni-directional	Omni-directional
Impedance	50 $\Omega$	50 $\Omega$
Size	6.0 $\times$ 4.0 $\times$ 1.5 mm <sup>3</sup>	



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# LTCC Applications

- Monolithic , Three-dimensional , Cost-effective
- Firing Temperature  $< 1000\text{ }^{\circ}\text{C}$
- Benefits :
  - flexibility , density , reliability , reduced weight , low-loss
- Better than thick-film process ( single-step )
- High performance in commercial and military use



# LTCC for Wireless Applications

- Base Station Amplifier Modules
- Transmitters and Receivers
- Handset Power Amplifiers
- Low Noise Amplifiers
- Voltage Control Oscillators
- Mixers
- Filters
- Power Splitters and Combiners
- Matching Networks



# LTCC in Military & Space Environments

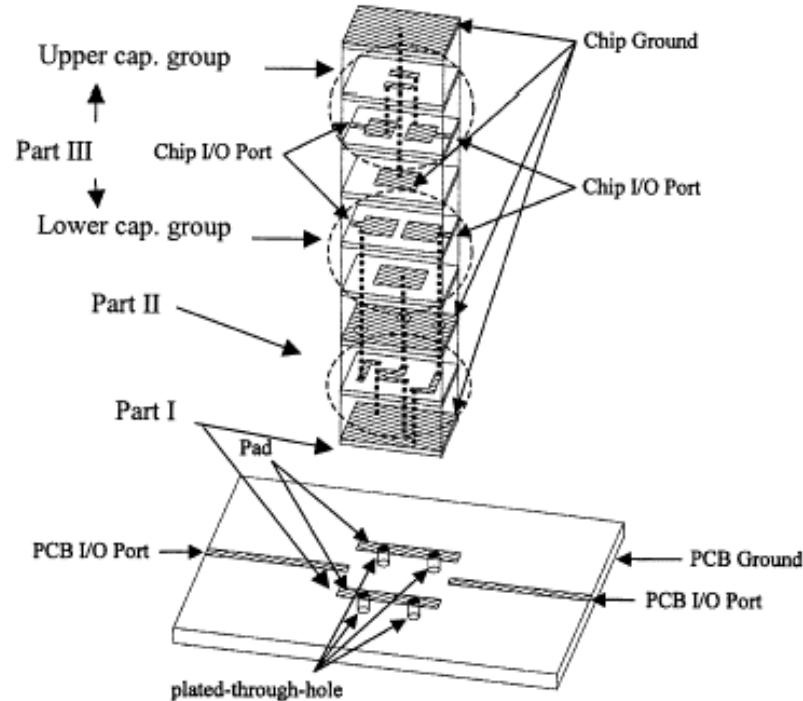
- Transmitters/Receivers
- Phased Array Radar
- Amplifiers
- Filters
- Converters
- Power Drivers
- Sensors



# LTCC in the Automotive Industry

- Engine Management Systems
- Gearbox Management Systems
- Anti-Lock Braking Systems
- Global Positioning Systems
- Gas Discharge Lamp Controllers
- Ignition Modules
- Sensor Modules

# Miniaturized LTCC Filters



(a)

- Reserve all the design advantage of strip line
- Can be use in portable telephone and other device



# Miniaturized RF Modules(1/3)

- Have a lower cost than conventional thick-film process
- Allow innovative implementation of circuit
- The ability to integrate L , R , C
- Incorporation with IC technology further opens a wide range of functionalities and modularization

# Miniaturized RF Modules(2/3)

## Material properties

- Layer thickness :  $25\mu\text{m}\sim 250\mu\text{m}$
- Layer count : 80 layers
- $\epsilon_r$  : 5~300
- $\tan\delta$  : 0.001~0.005
- Silver has been extensively used as conductors
- Surface material : platinum , palladium , silver , gold

# Miniaturized RF Modules(3/3)

## Advantages

- Reduced size (1/2)
- Reduced cost (1/4)
- Key improvement :

impedance matching between circuits or module

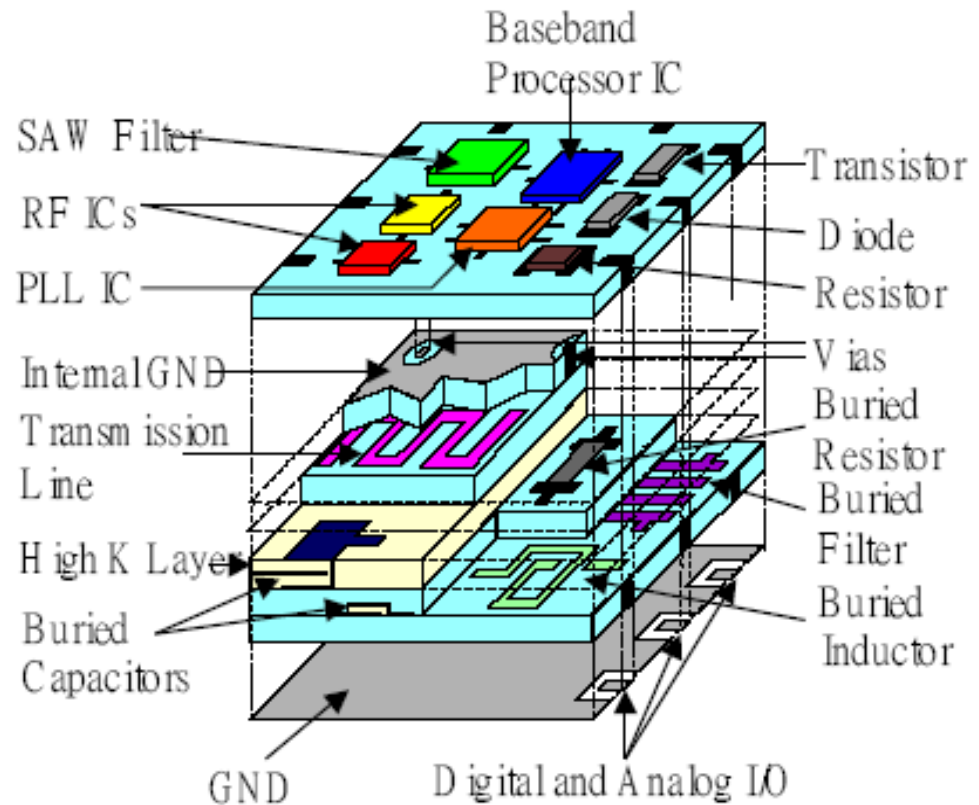
⇒ improve the performance and power efficiency of PA

⇒ **longer battery life or smaller battery size**



# LTCC Module

- \*Buried passive components
- \*Substrate as package (cavity...)
- \*Lower TCE (match to Si and GaAs)
- \*Smaller module volume
- \*Packaging capability (BGA, FC...)





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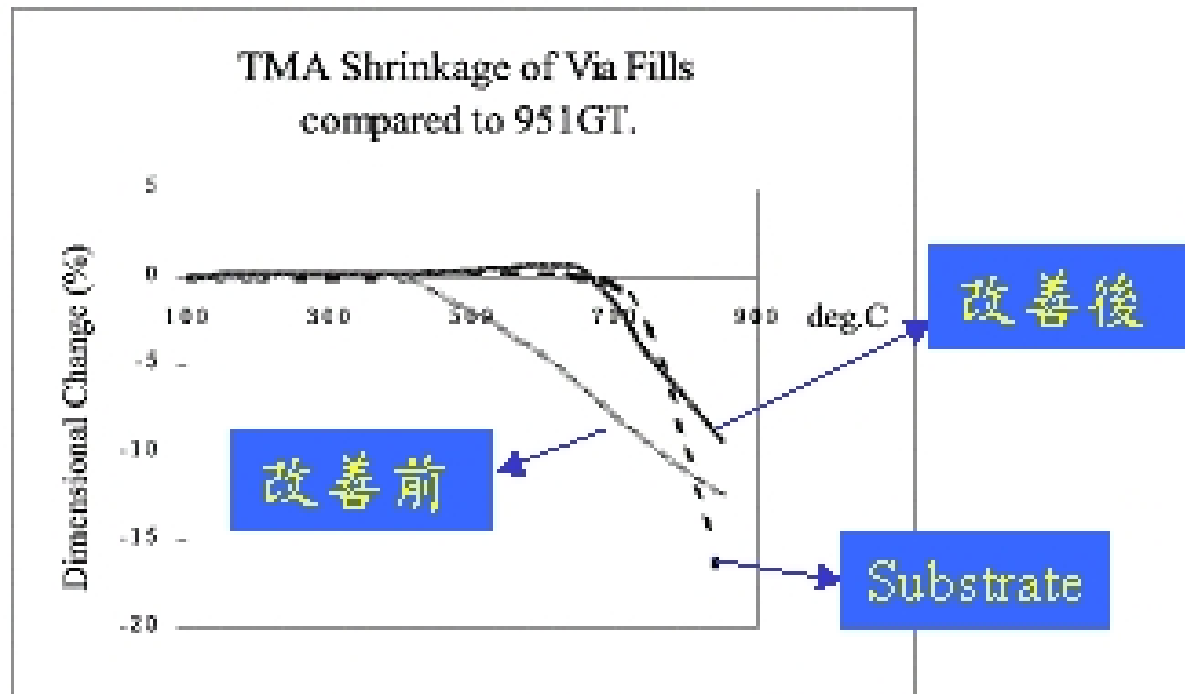


# Future developments

- Zero shrinking
- High-permittivity dielectric pastes
- Buried (active) components
- TB-BGA
- Optical components
- Liquid and gas interfaces / conductors
- Brick box system

# Zero shrinking

共燒收縮匹配(延遲燒結)



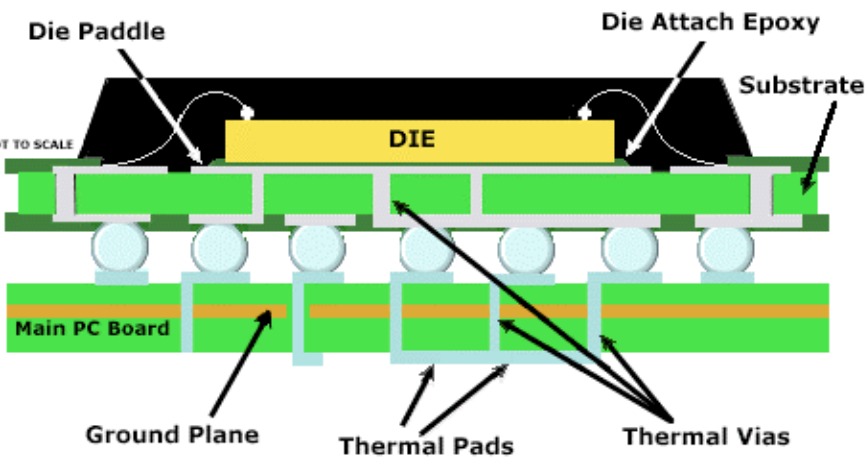
Ref.:2001 IMAPS proceeding

不同填孔膠之燒結收縮曲線

改善前：添加填孔膠為收縮製程使用

改善後：添加填孔膠為不收縮製程使用

# TB-BGA



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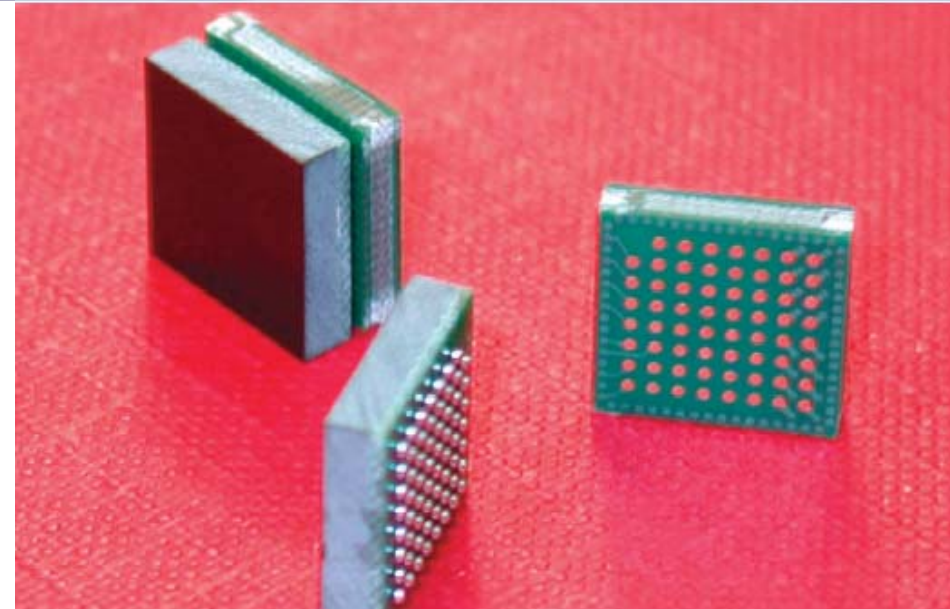
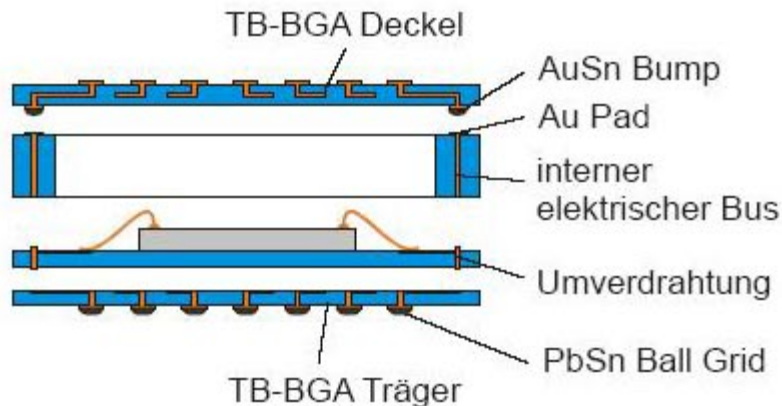


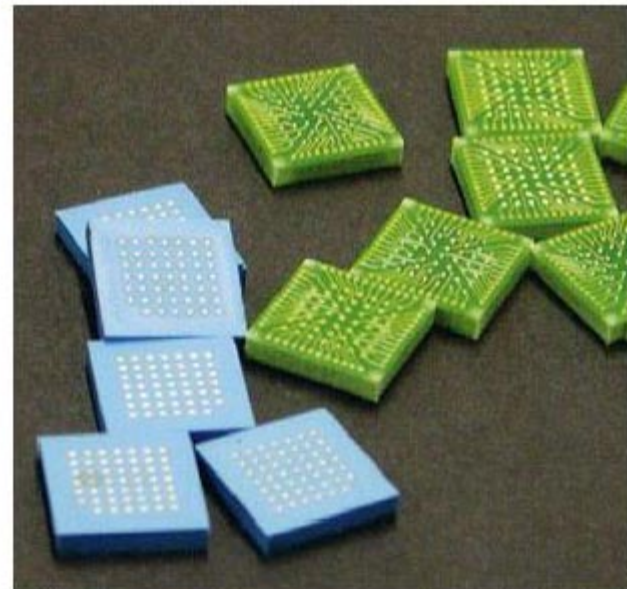
Bild 1: Match-X-Stromsensor- und Signalkonditionierungsbaustein; jeweils einzeln und als Stack (links oben)

[http://www.mstonline.de/publikationen/infoboerse/ib\\_2003/ib42.pdf](http://www.mstonline.de/publikationen/infoboerse/ib_2003/ib42.pdf)

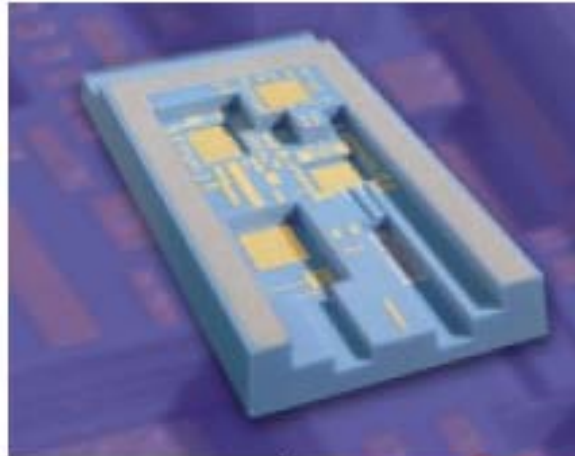
- Low Temperature Cofired Ceramics (LTCC) (siehe Photo, links)
- FR4-Platinenwerkstoff (siehe Photo, rechts)



[http://www.imtek.uni-freiburg.de/mikroelektronik/content/upload/system\\_04.pdf](http://www.imtek.uni-freiburg.de/mikroelektronik/content/upload/system_04.pdf)



# Optical components



3D LTCC Cavity System



Precision Fibre Alignment

When formulating a new optical product, one of the most critical decisions is the choice of **package**.



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# **Realization of Transmission Zeros in Compline Filters Using an Auxiliary Inductively Coupled Ground Plane**

Ching-Wen Tang,

Yin-Ching Lin,

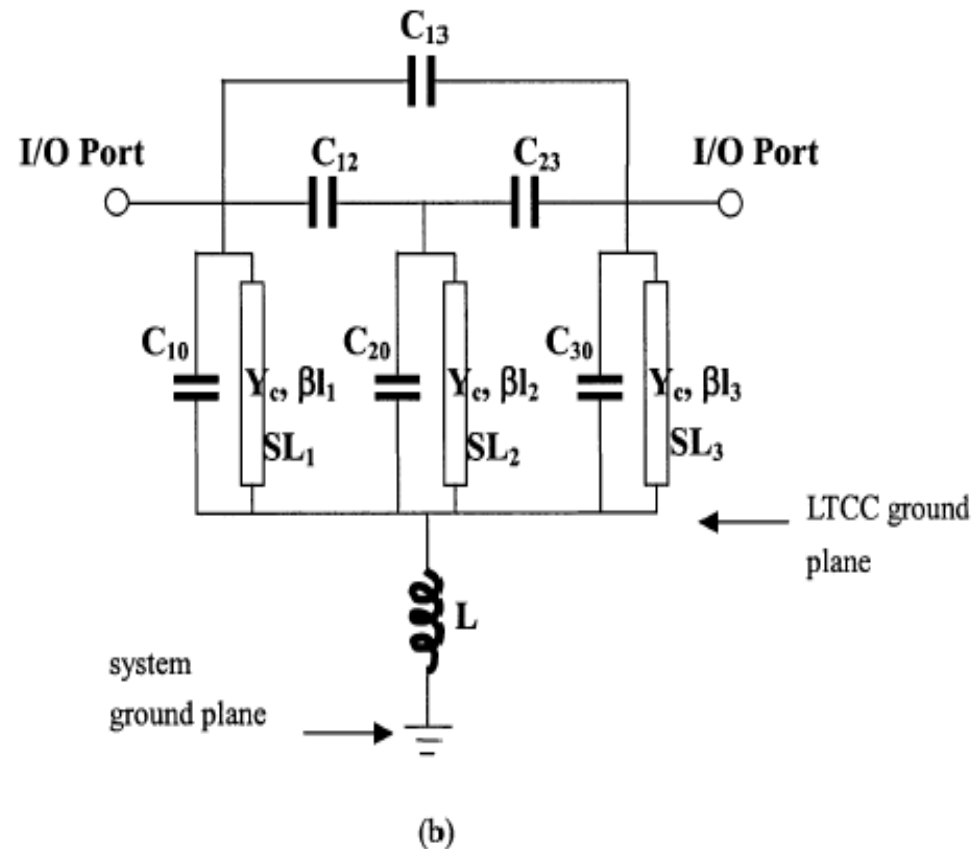
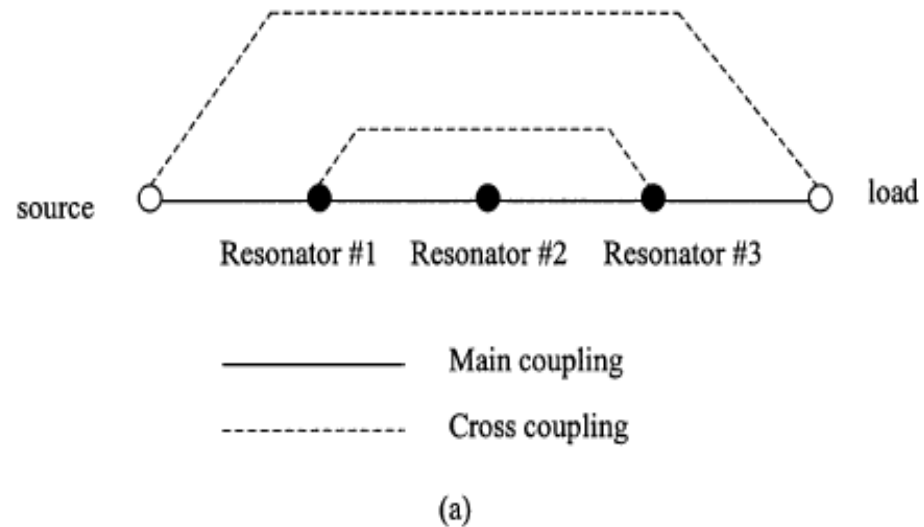
Chi-Yang Chang

IEEE TRANSACTIONS ON MICROWAVE THEORY AND TECHNIQUES,  
VOL. 51, NO. 10, OCTOBER 2003

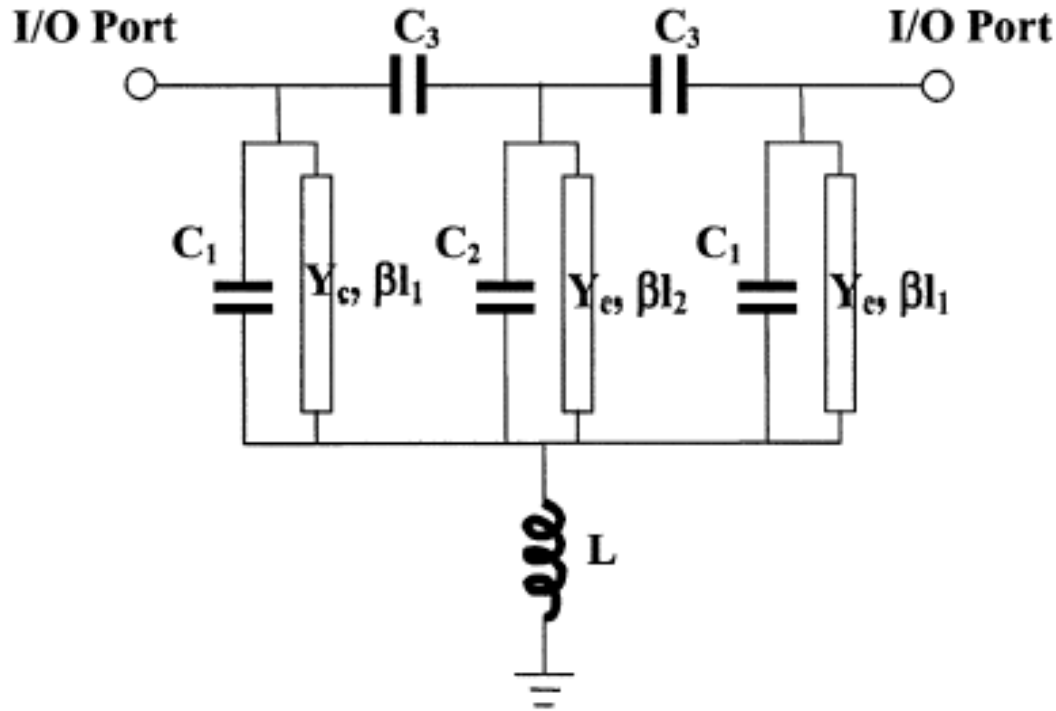


# Introduction

- ◆ Inductive coupling among three resonator
- ◆ Three pole combine filter with capacitive cross-coupling between I/O ports
- ◆ Generate two transmission zeros at a low-side skirt to reject local and image signals.
- ◆ For the high-side skirt , the inductance generates an extra transmission zero to suppress the harmonic frequency.
- ◆ By tuning the  $L$  and  $C_{13}$  properly, three transmission zeros appeared at proper places.



# Derivation of The Y Matrix



(a)



(b)

$$l_1 = l_3$$

$$C_{10} = C_{30} = C_1 = 4.48 \text{ pF}$$

$$C_{20} = C_2 = 2.16 \text{ pF}$$

$$C_{12} = C_{23} = C_3 = 0.77 \text{ pF}$$

$$C_{13} = C_4 = 0.36 \text{ pF}$$

Size of  $SL_{1,3}$

$$= 74 \text{ mil} * 8 \text{ mil}$$

Size of  $SL_2$

$$= 115 \text{ mil} * 8 \text{ mil}$$

$$L = 0.04 \text{ nH}$$

$$\epsilon_r = 7.8$$

# Derivation of The Y Matrix

$$\begin{aligned} Y_{11} &= Y_{22} \\ &= Y_{C4} \\ &\quad + \frac{Y_{C3}^2 + (1 + Y_{C3}Z_L + Y_1Z_L) \cdot [Y_2Y_{C3} + Y_1(Y_2 + 2Y_{C3})]}{2Y_{C3} + 4Y_1Y_{C3}Z_L + Y_2(1 + 2Y_{C3}Z_L + 2Y_1Z_L)} \\ &= \frac{Y_{N1}}{Y_D} \end{aligned} \quad (1)$$

$$\begin{aligned} Y_{12} &= Y_{21} \\ &= -Y_{C4} - \frac{Y_{C3}^2 + Z_L(Y_1 + Y_{C3}) \cdot [Y_2Y_{C3} + Y_1(Y_2 + 2Y_{C3})]}{2Y_{C3} + 4Y_1Y_{C3}Z_L + Y_2(1 + 2Y_{C3}Z_L + 2Y_1Z_L)} \\ &= \frac{Y_{N2}}{Y_D} \end{aligned} \quad (2)$$

$$Y_1 = j(\omega C_1 - Y_C \cot(\beta l_1))$$

$$Y_2 = j(\omega C_2 - Y_C \cot(\beta l_2))$$

$$Y_3 = j(\omega C_3 - Y_C \cot(\beta l_3)) = Y_1$$

$Z_L$  is the impedance of inductor

$Y_{C3}$  is the admittance of capacitor  $C_3$

$Y_{C4}$  is the admittance of capacitor  $C_4$

# Prediction of The Transmission Zeros by Y Matrix

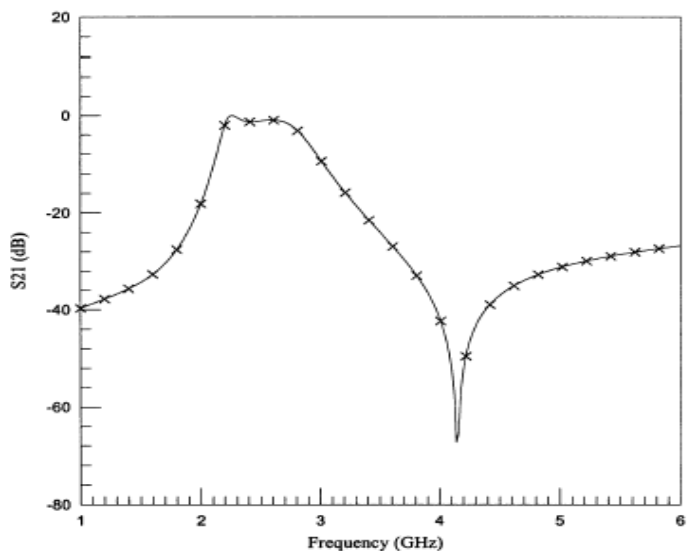


Fig. 3. Response of the filter in Fig. 2(a) with the transmission zero located at

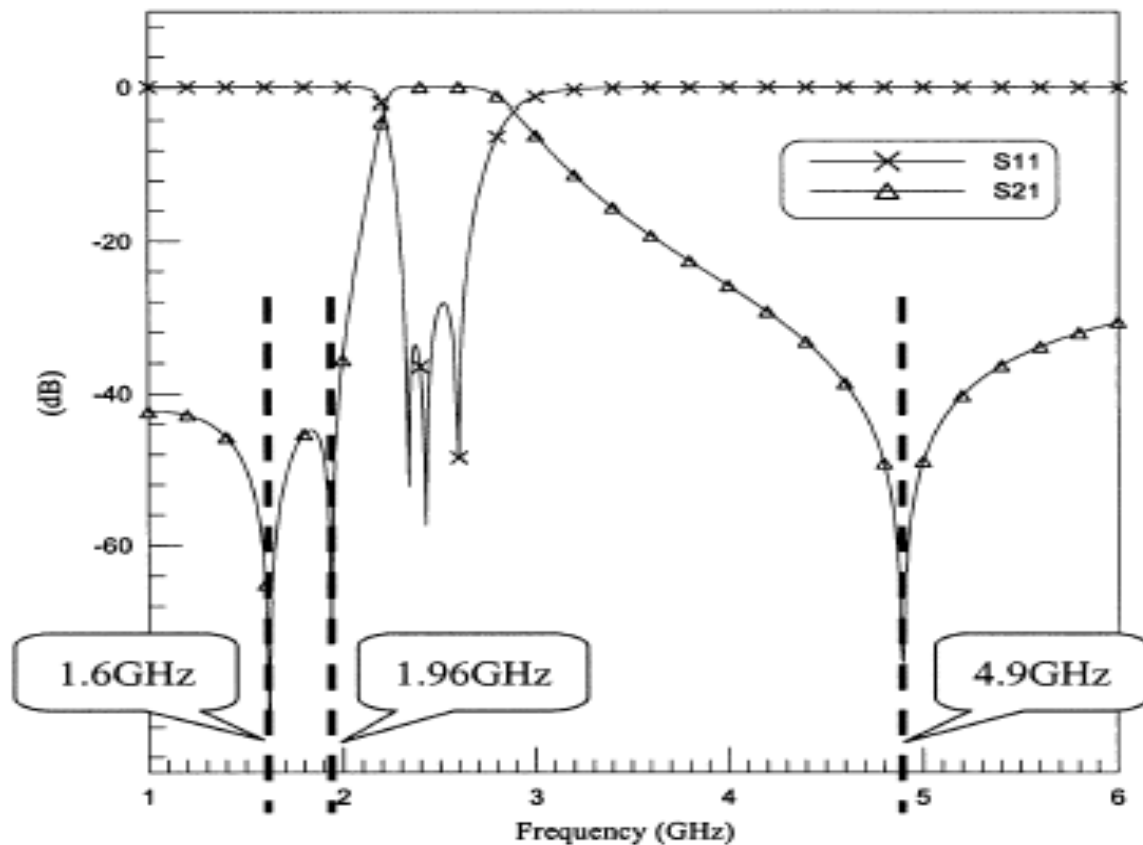
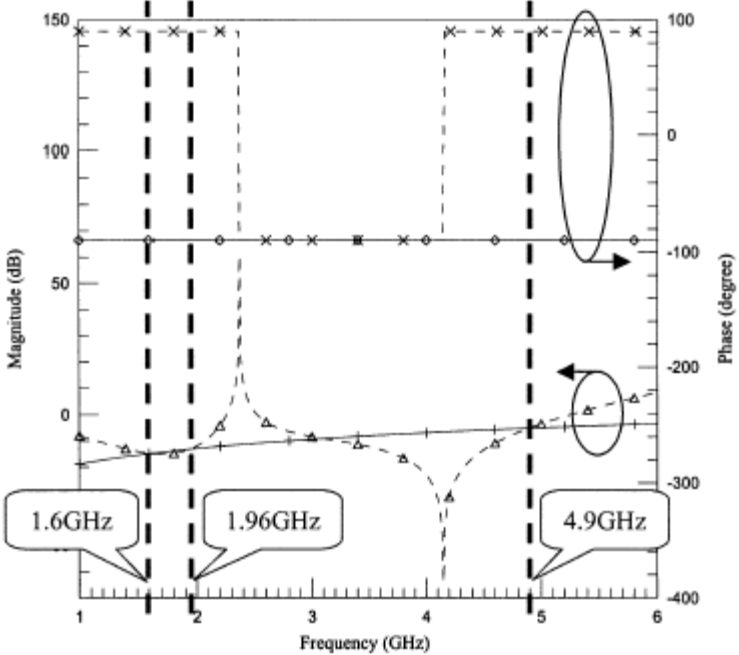
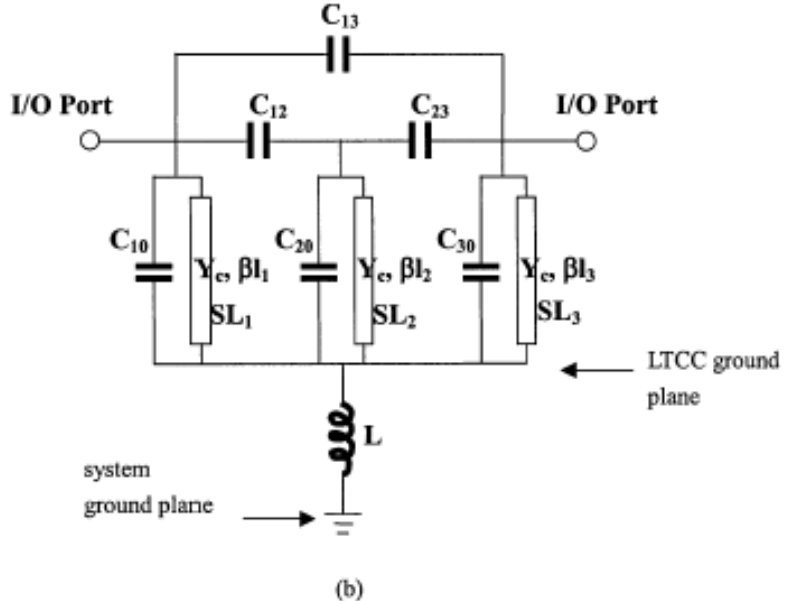
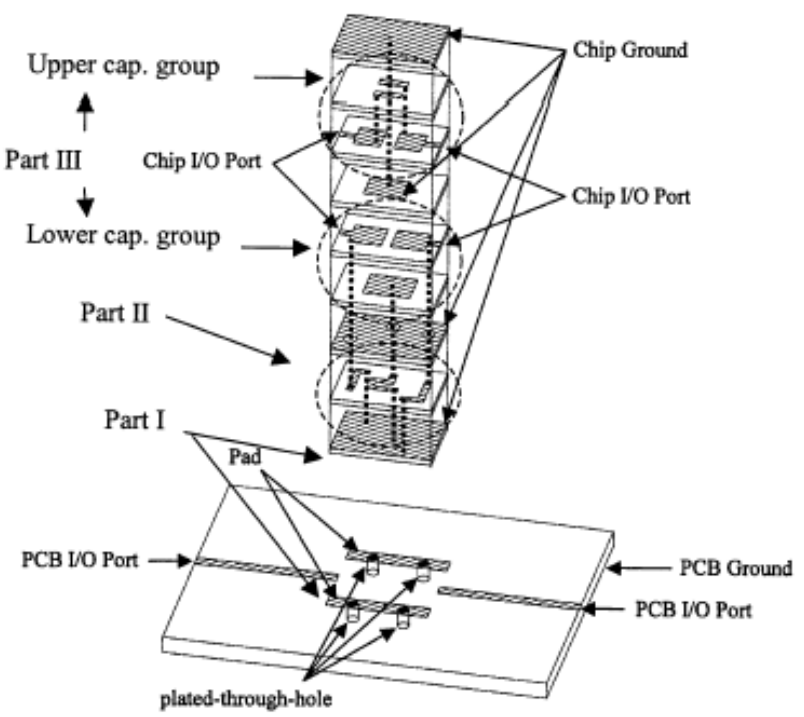


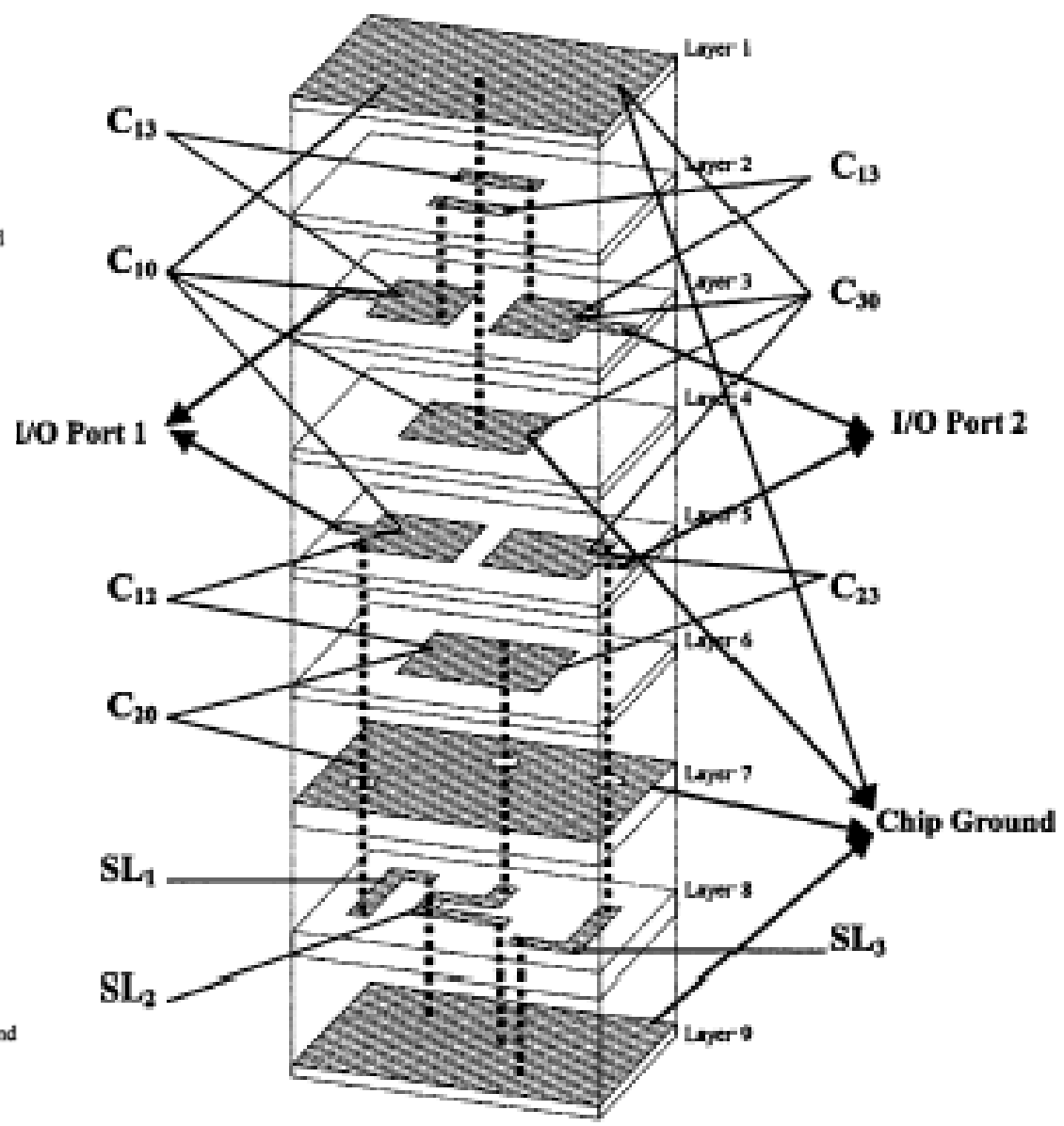
Fig. 5. Simulated result of the multilayer LTCC bandpass filter.



(b)

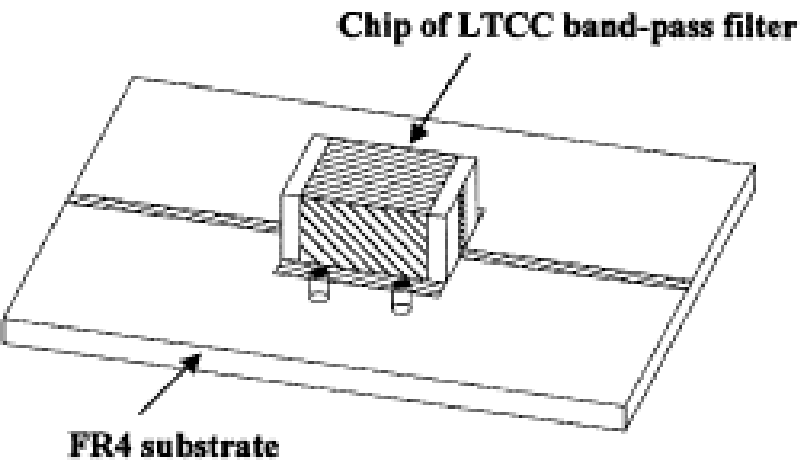


(a)



(b)

# EM simulation by HFSS



FR4 PCB  
 $t = 0.4 \text{ mm}$   
 $\epsilon_r = 4.47$

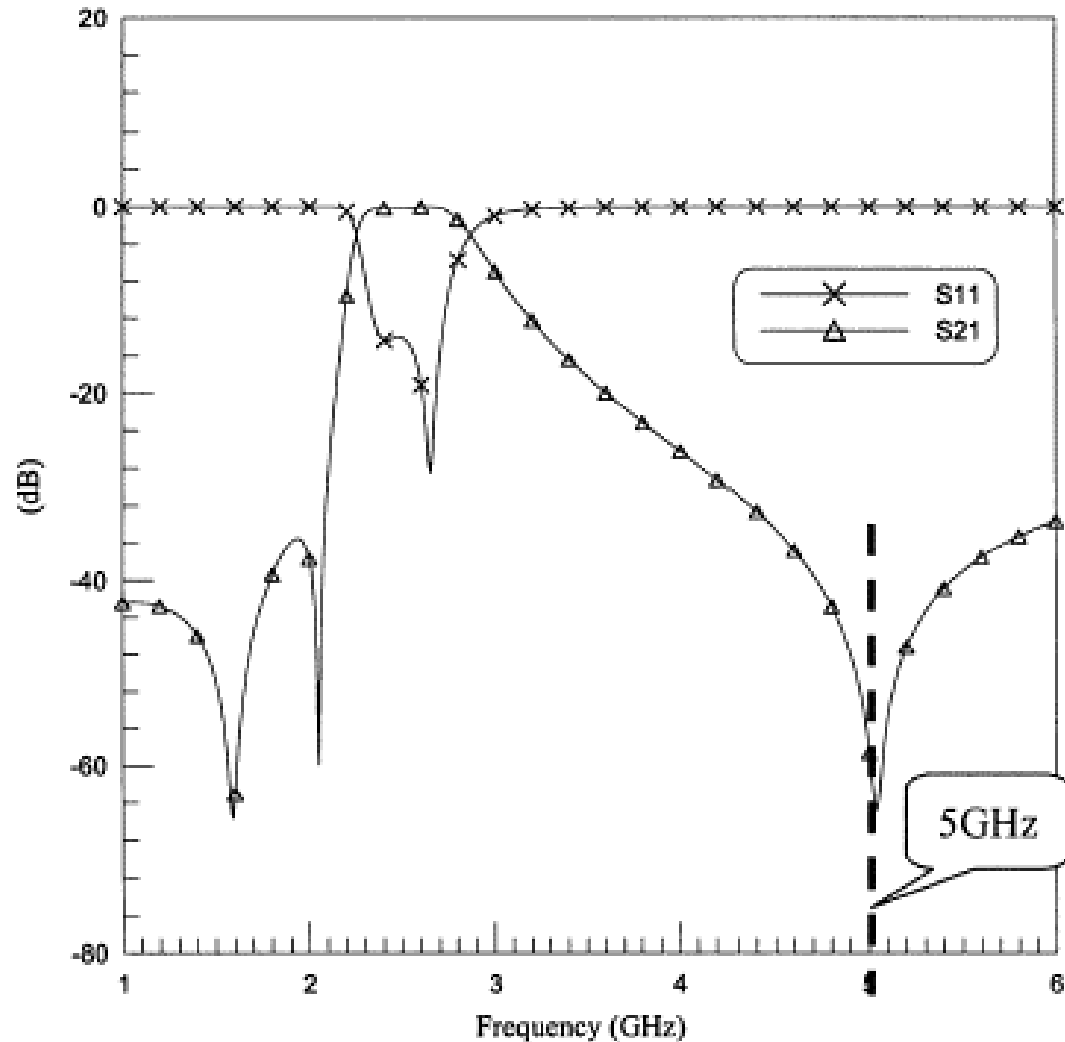
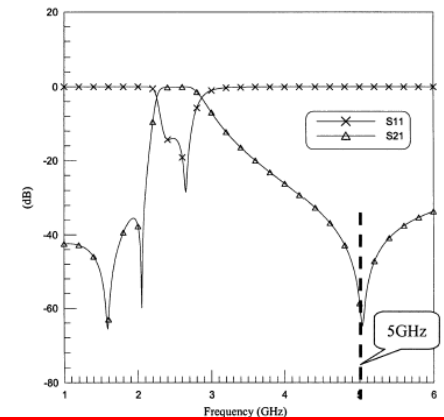
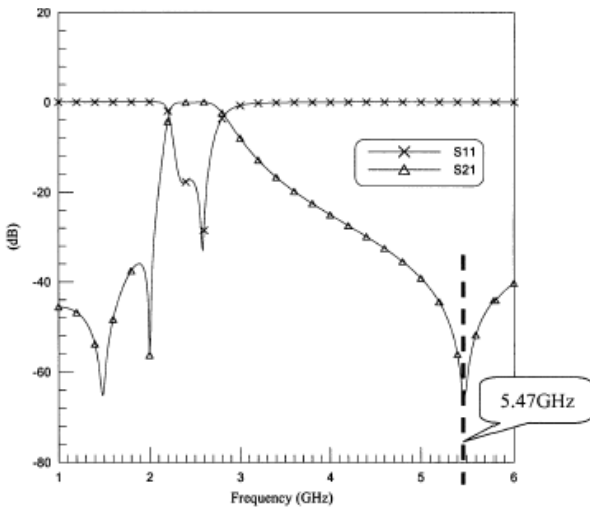
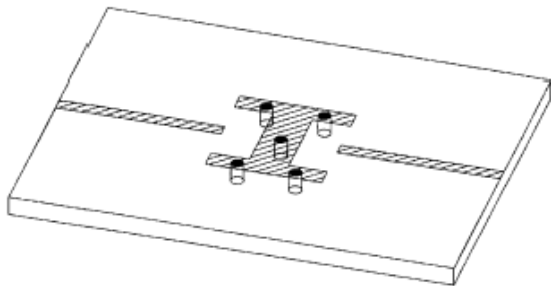


Fig. 7. Simulated response of an LTCC filter mounted on a PCB, as shown in Fig. 6(c).

# Analysis of Three Parasitic

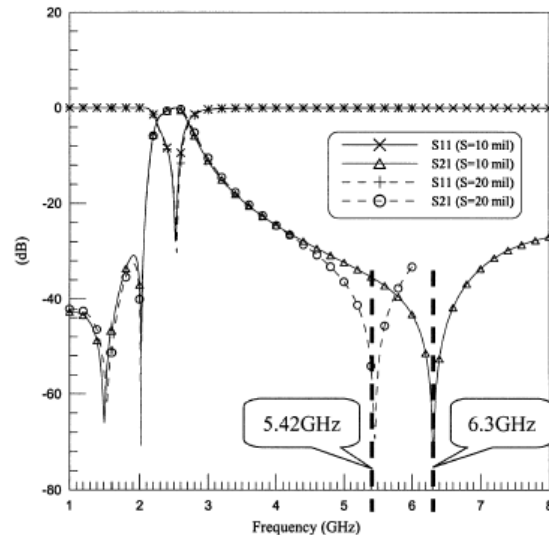
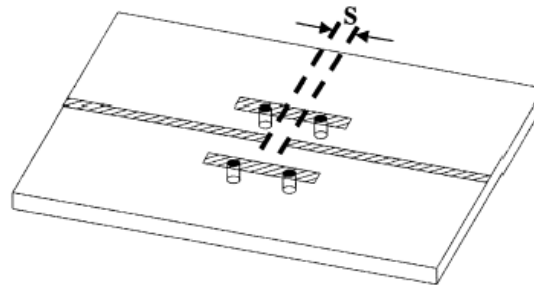


1) Through-hole inductance

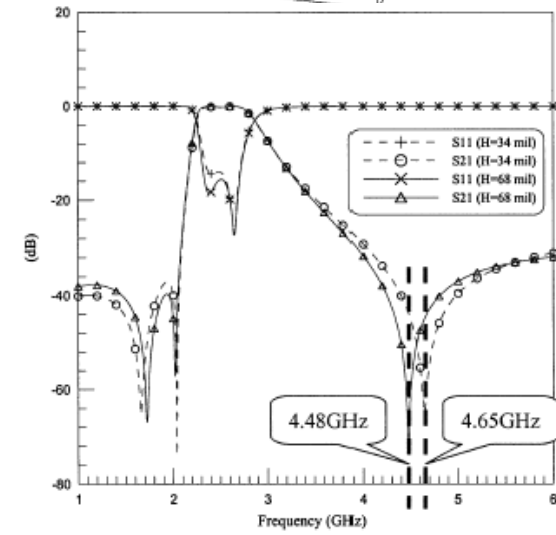
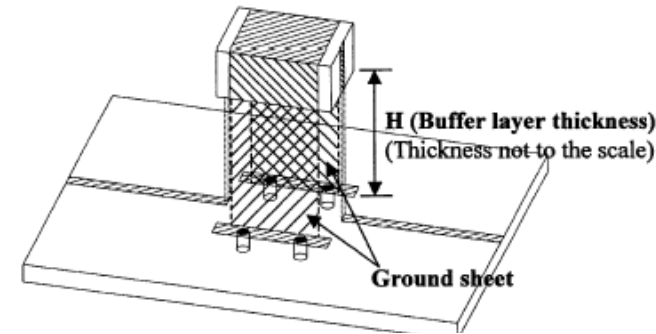


(b)

2) Microstrip gap

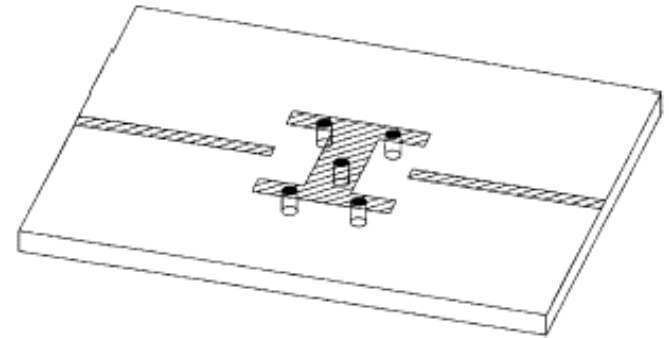


3) Buffer layer thickness



# Analysis of Three Parasitic Effects- *Through-hole inductance*

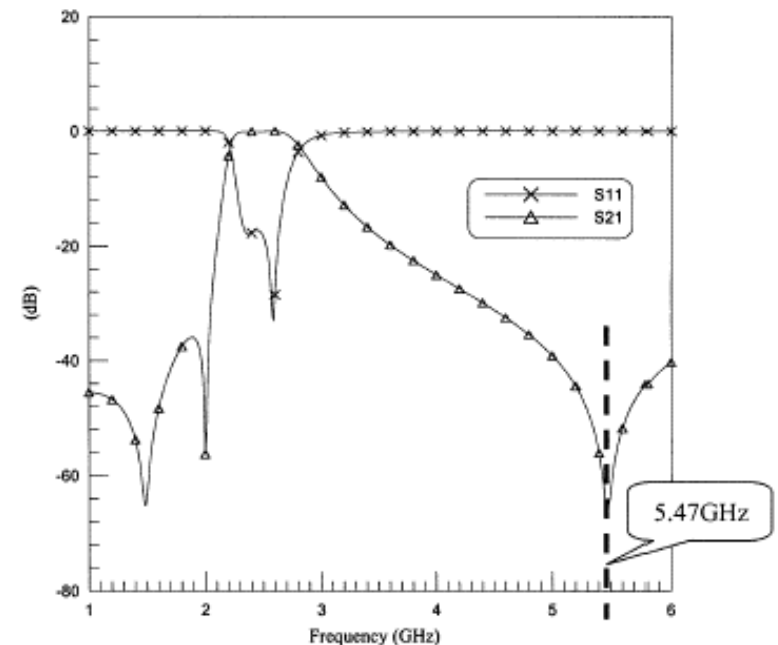
- 4 holes : 5.00 GHz
- 5 holes : 5.47 GHz



$$\text{holes} \propto \frac{1}{L}$$

$$L \propto \frac{1}{f_{\text{zero}}}$$

$$\text{holes} \propto f_{\text{zero}}$$

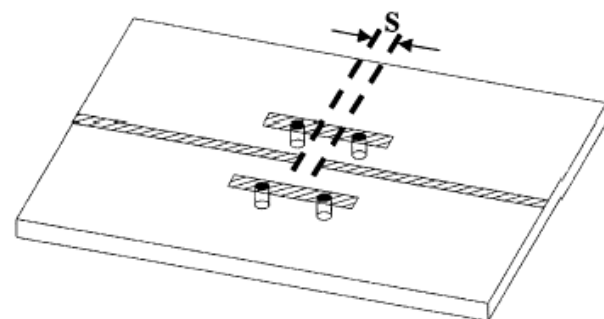


(b)



# Analysis of Three Parasitic Effects- *Microstrip gap*

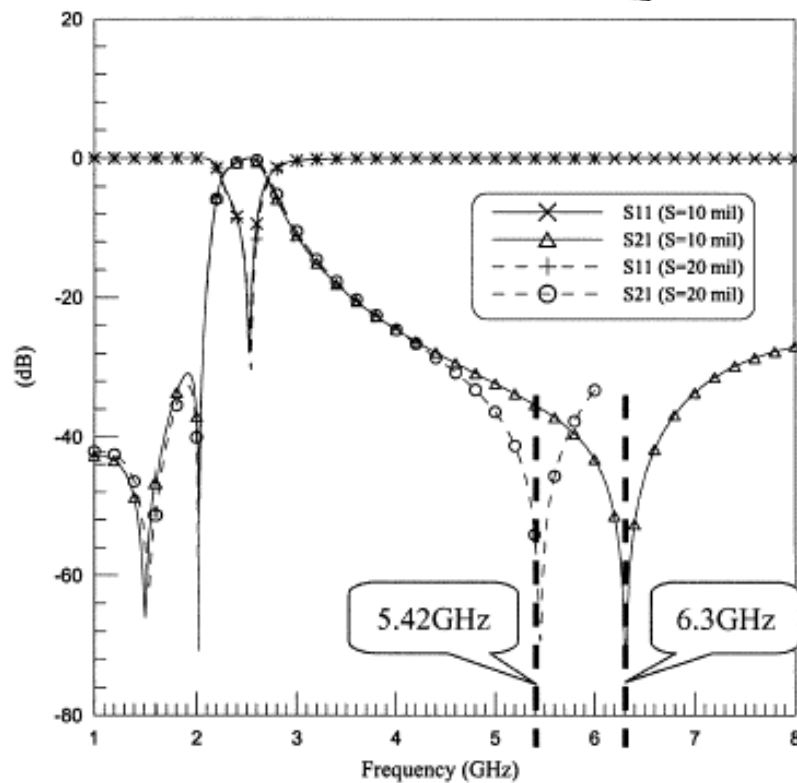
- 20 mil : 5.42 GHz
- 10 mil : 6.30 GHz



$$S \propto \frac{1}{C}$$

$$C \propto f_{zero}$$

$$S \propto \frac{1}{f_{zero}}$$



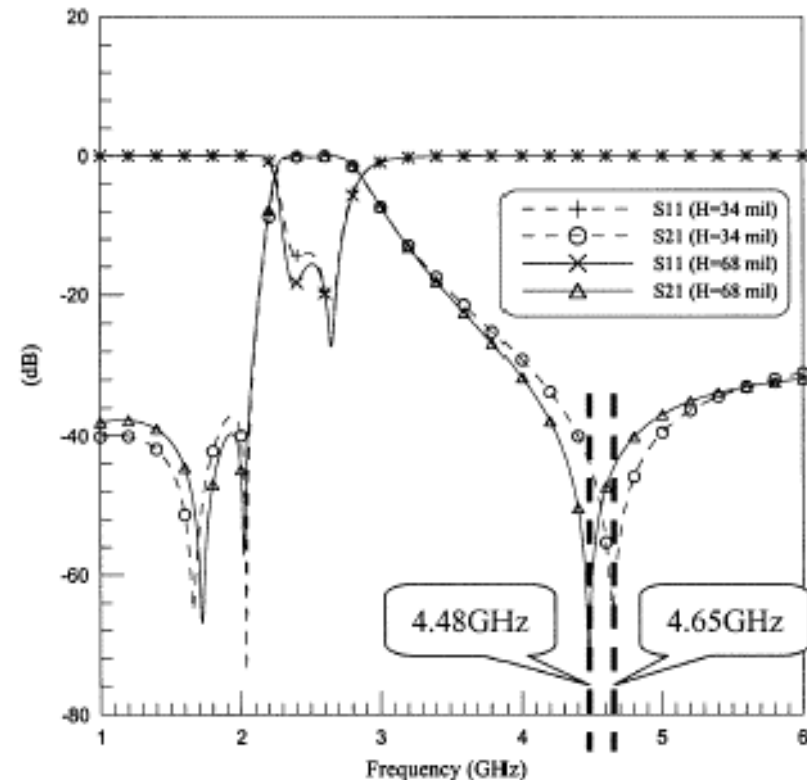
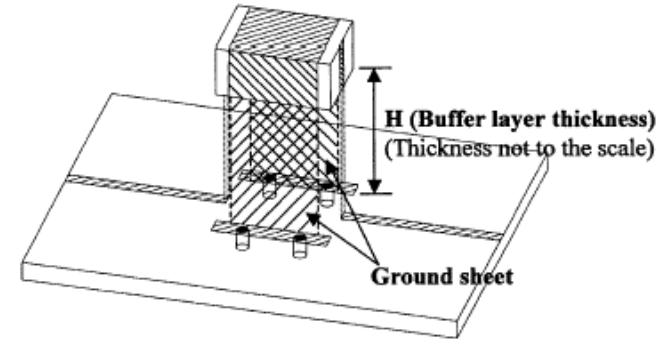
# Analysis of Three Parasitic Effects- *Buffer layer thickness*

- H=34 mil : 4.65 GHz
- H=68 mil : 4.48 GHz

$$H \propto L$$

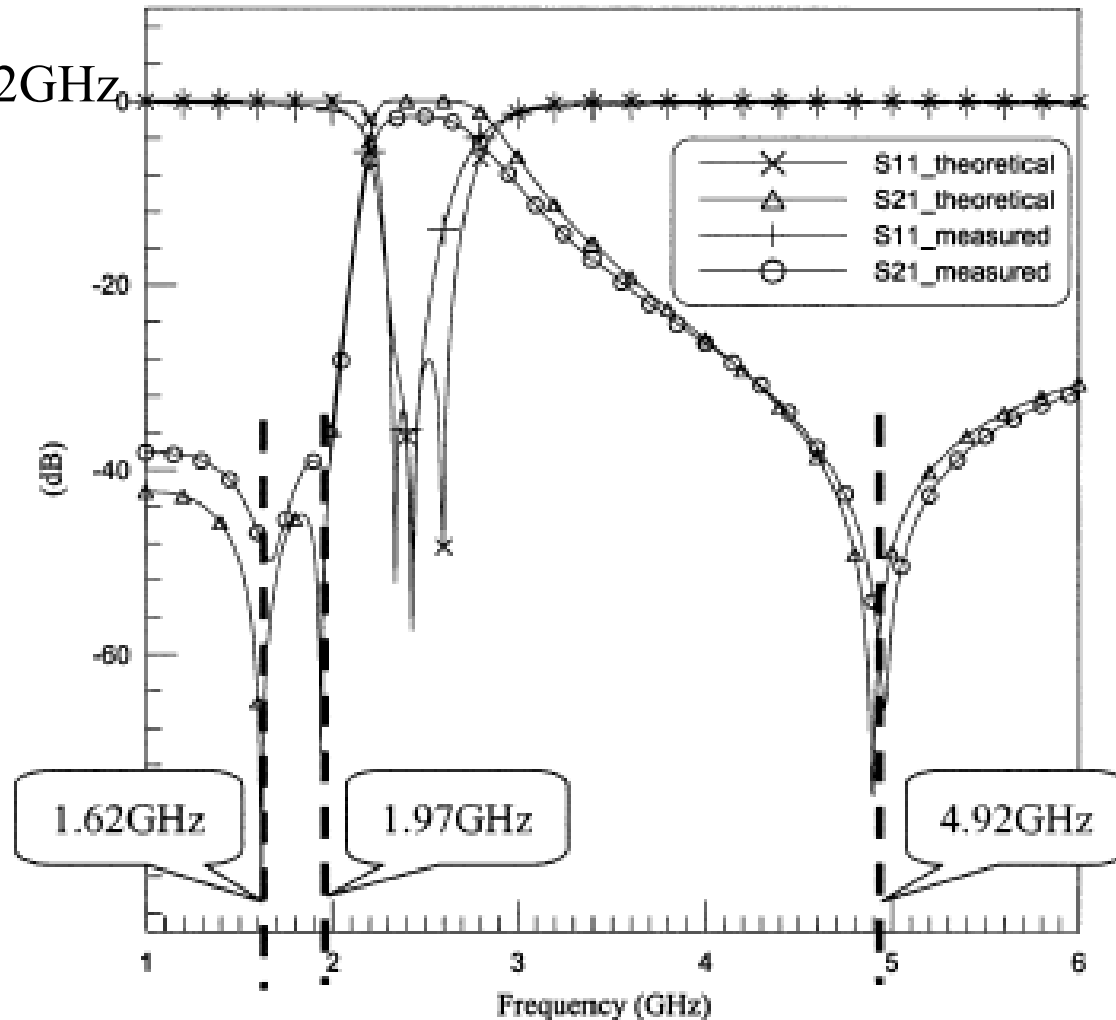
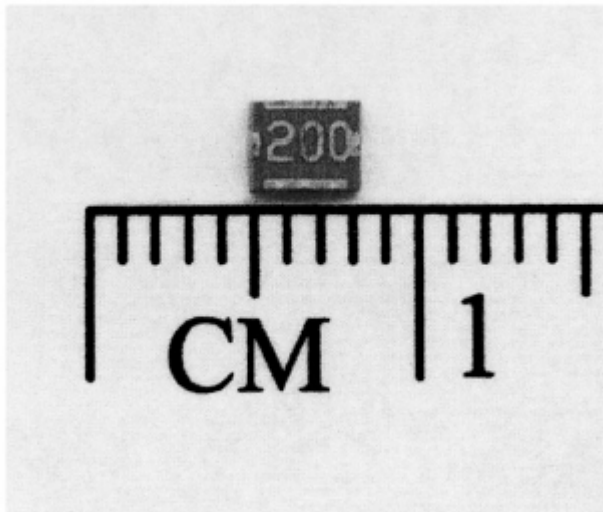
$$L \propto \frac{1}{f_{zero}}$$

$$H \propto \frac{1}{f_{zero}}$$



# MEASURED RESULTS

- ◆ Dupont951  $\epsilon_r=7.8$  ;  $\tan\theta=0.0045$
- ◆ Buffer layer thickness = 3.6 mil
- ◆ Chip size = 3.2mm\*2.5mm\*1.2mm
- ◆ IL<1.67dB
- ◆ Zeros = 1.62GHz;1.97GHz;4.92GHz
- ◆ Metal thickness=5 $\mu\text{m}$





# Design of a 2-Pole LTCC Filter for Wireless Communications

Vadim Piatnitsa ,  
Eino Jakku ,  
Seppo Leppaevuori

# FILTER DESIGN

## *Filter Specification*

- Pass Band : 1.9 GHz~ 2.0 GHz
- $f_o$  : 1950 MHz
- BW : 5 %
- IL : < 2 dB
- OBR<sub>low</sub> : >20 dB (1.58~1.64 GHz)
- OBR<sub>up</sub> : >10 dB (1.75~1.81 GHz)

# FILTER DESIGN

## *Filter Synthesis*

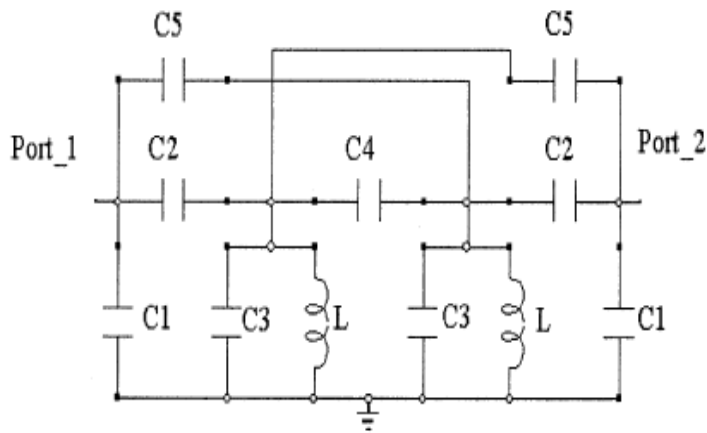


Fig. 1. The equivalent scheme of the second- order filter with cross coupling.

TABLE I  
KEY PARAMETERS OF THE EQUIVALENT SCHEME

C1, pF	C2, pF	C3, pF	C4, pF	C5, pF	L, nH
0.2	0.5	1	0.1	0.1	4.2

2-pole filter      Chebyshev prototype

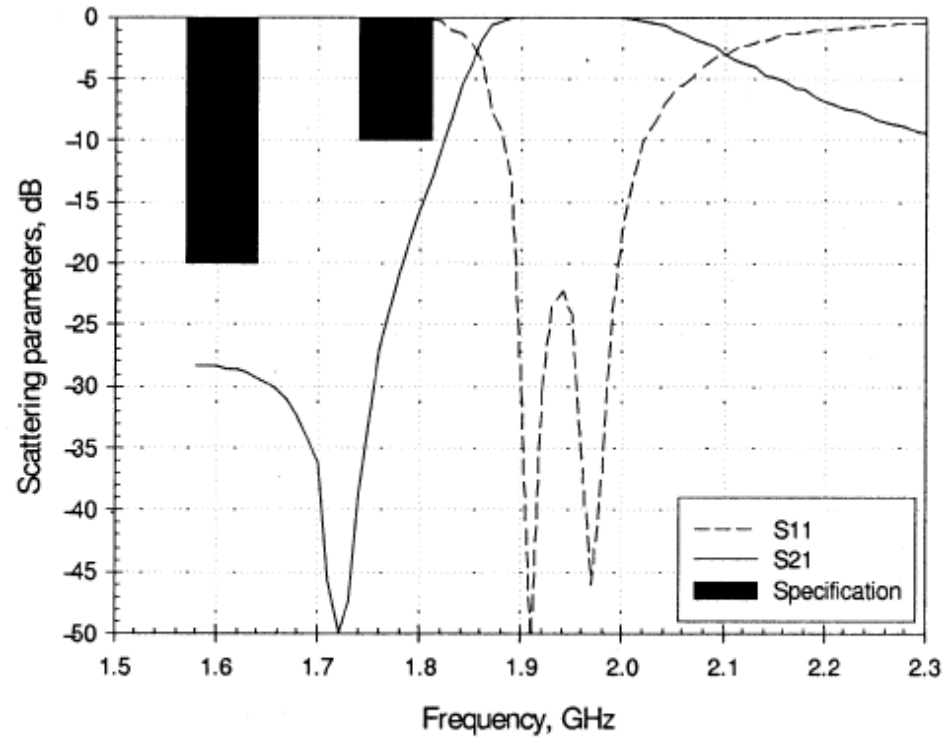


Fig. 2. The frequency response of the equivalent circuit.

# FILTER DESIGN

## *Physical Realization of the Filter*

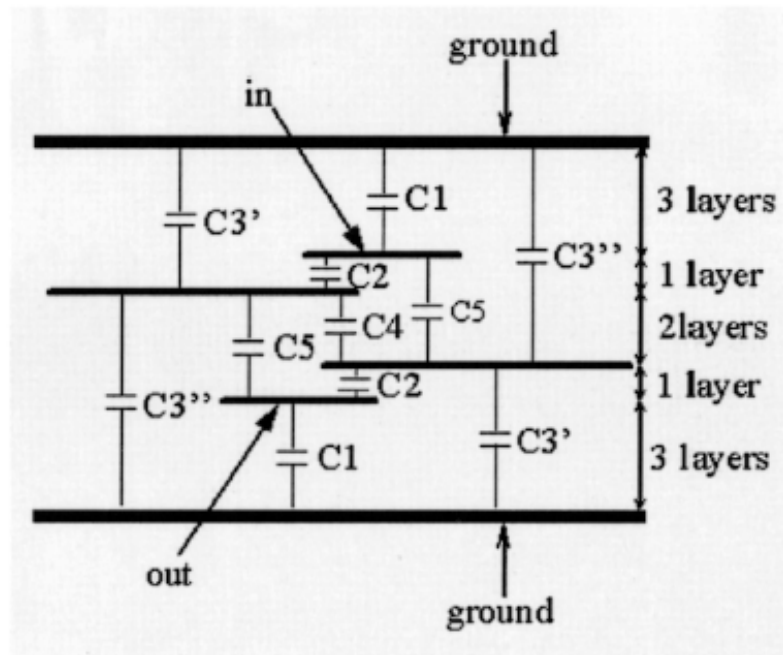


Fig. 3. The physical realization of capacitances.

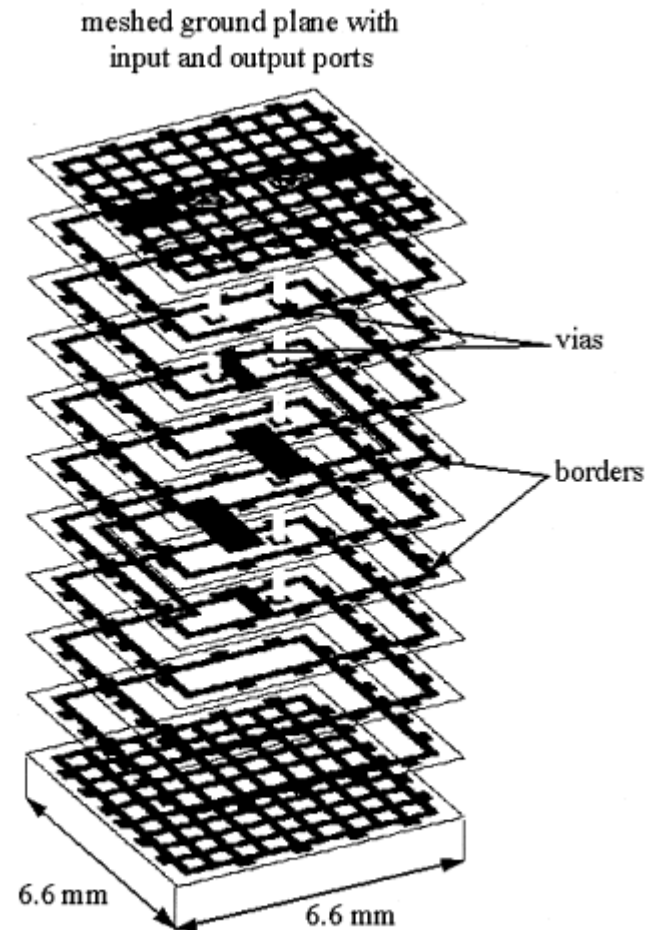


Fig. 4. The 3-D filter structure without vias between ground planes.

# FILTER DESIGN

## *Simulation*

- $\epsilon_r = 9.2 \pm 0.1$
- $\tan \theta = 0.002$
- $t = 99.1 \pm 2.5 \mu\text{m}$
- $t_c = 10 \mu\text{m}$
- shrinkage at x,y = 12.3%
- shrinkage at z = 15.6%

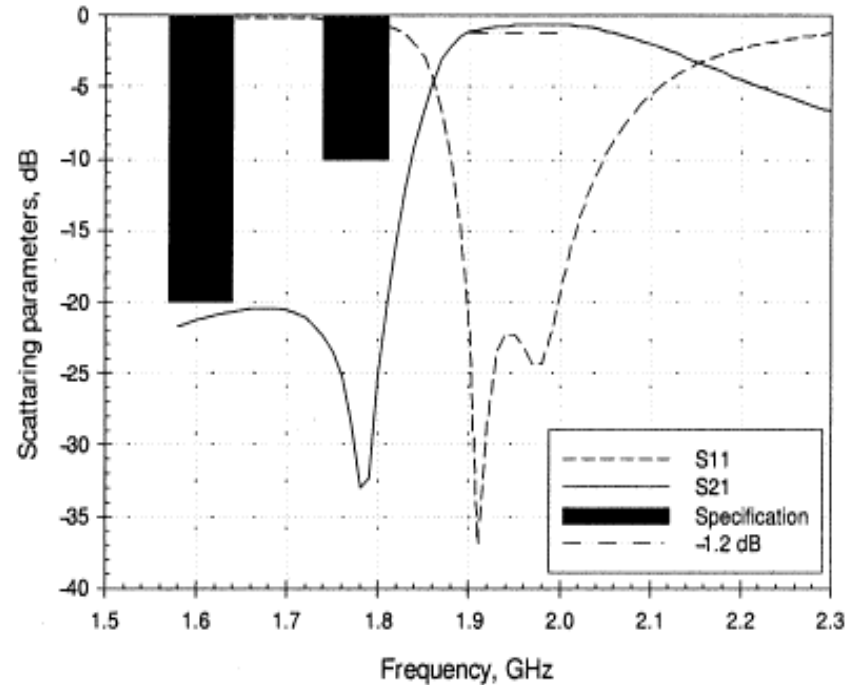


Fig. 5. The simulated filter.



# FILTER DESIGN

## *Measurement*

- $RL$  :  $> 13$  dB
- $IL$  :  $< 1.9$  dB
- $OBR_{low}$  :  $> 23$  dB
- $OBR_{up}$  :  $> 10$  dB
- Size :  $6.6 \times 6.6 \times 0.836$  mm<sup>3</sup>

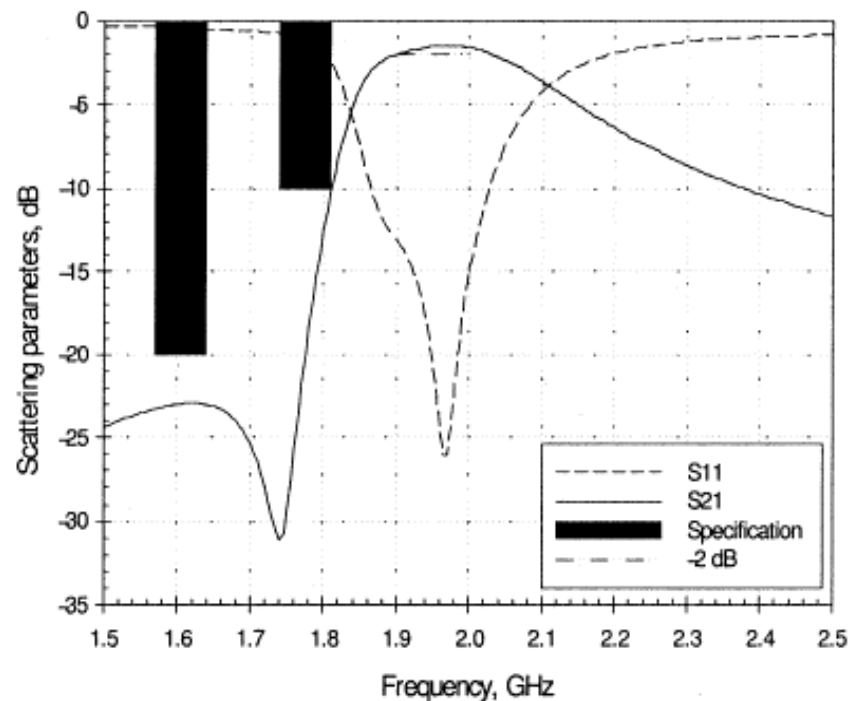
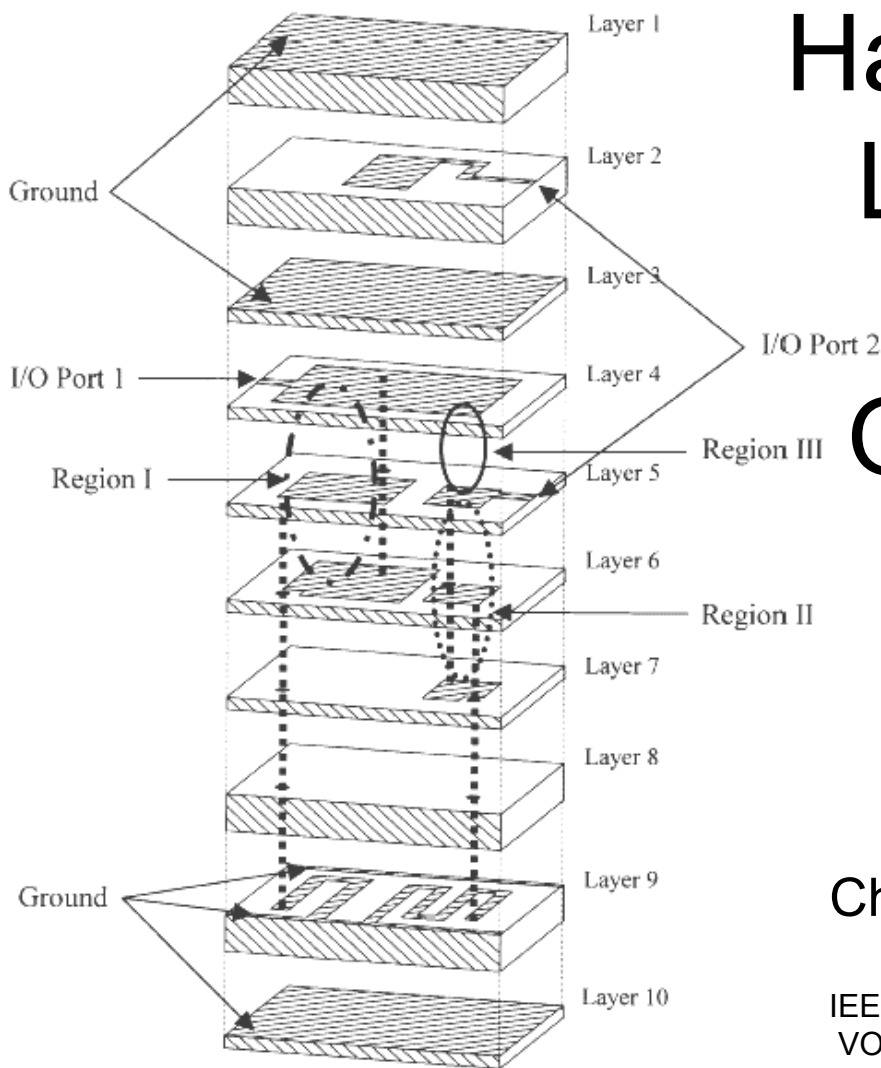


Fig. 6. The measured performance of a designed multilayered LTCC filter.



# Harmonic-Suppression LTCC Filter with the Step-Impedance Quarter-Wavelength Open Stub

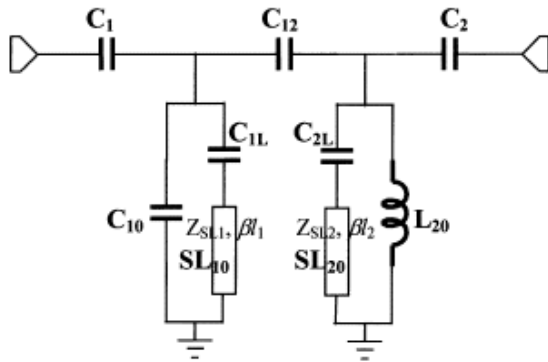
Ching-Wen Tang

IEEE TRANSACTIONS ON MICROWAVE THEORY AND TECHNIQUES,  
VOL. 52, NO. 2, FEBRUARY 2004

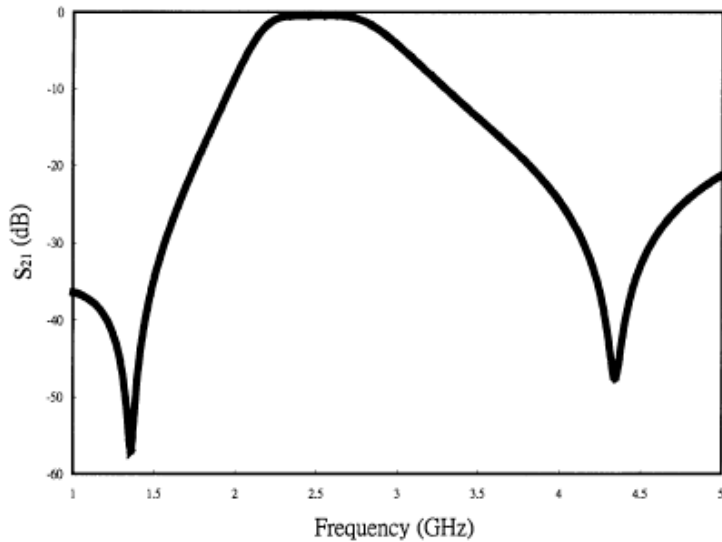
# Filter desired specifications

- Pass Band : 2.4 ~ 2.483 GHz
- IL : < 2 dB
- Zero<sub>lower</sub> : 1.96 and 2.1 GHz
- Zero<sub>upper</sub> : 4.8–5 GHz

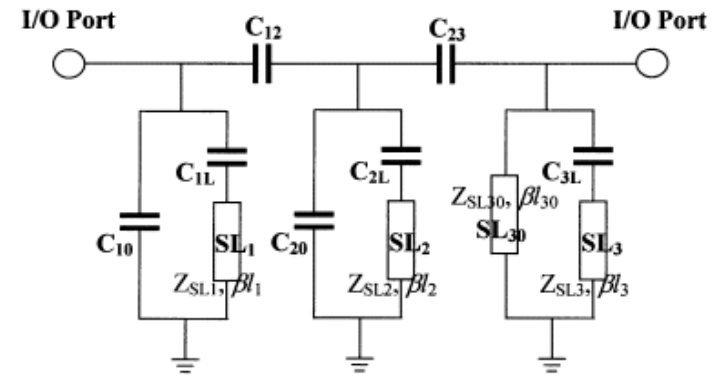
# Filter constructions



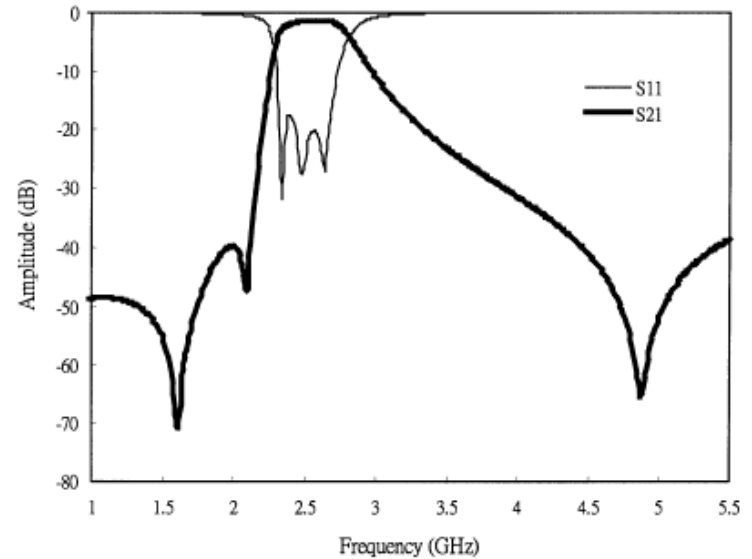
(a)



(b)

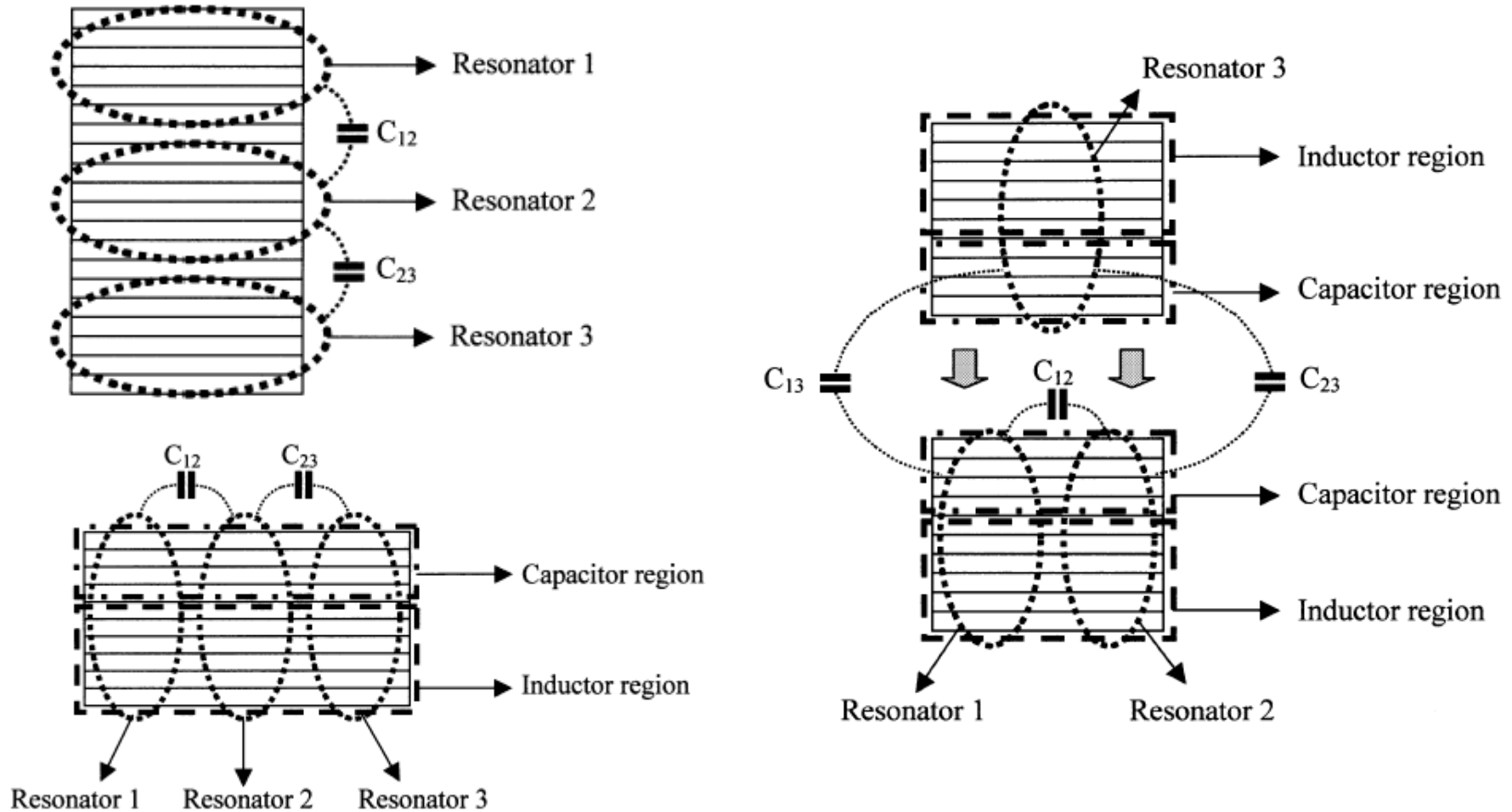


(a)

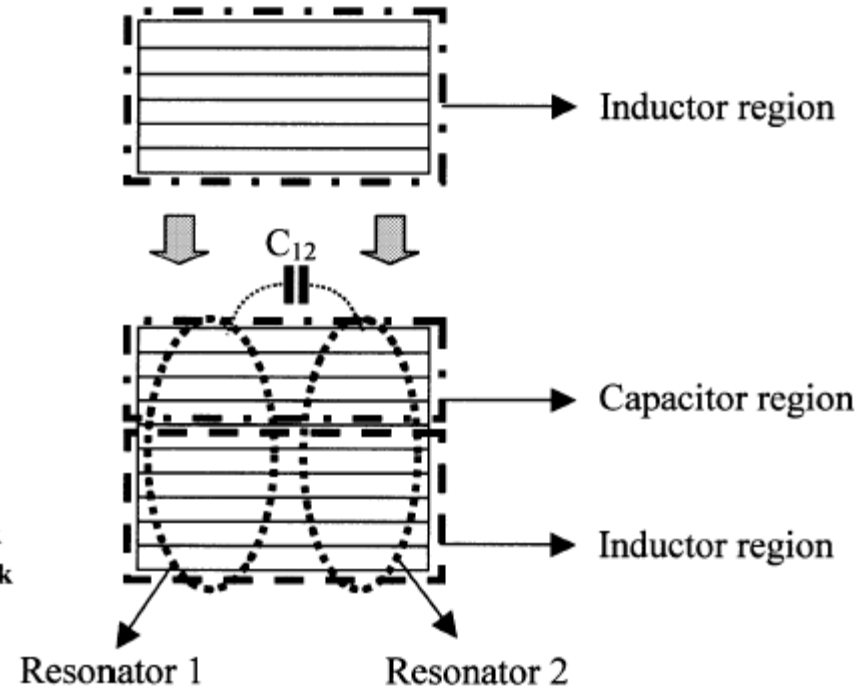
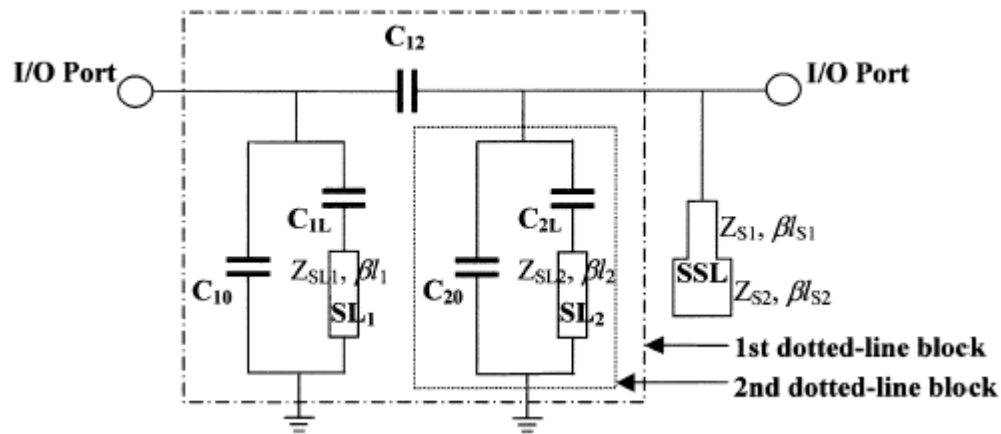


(b)

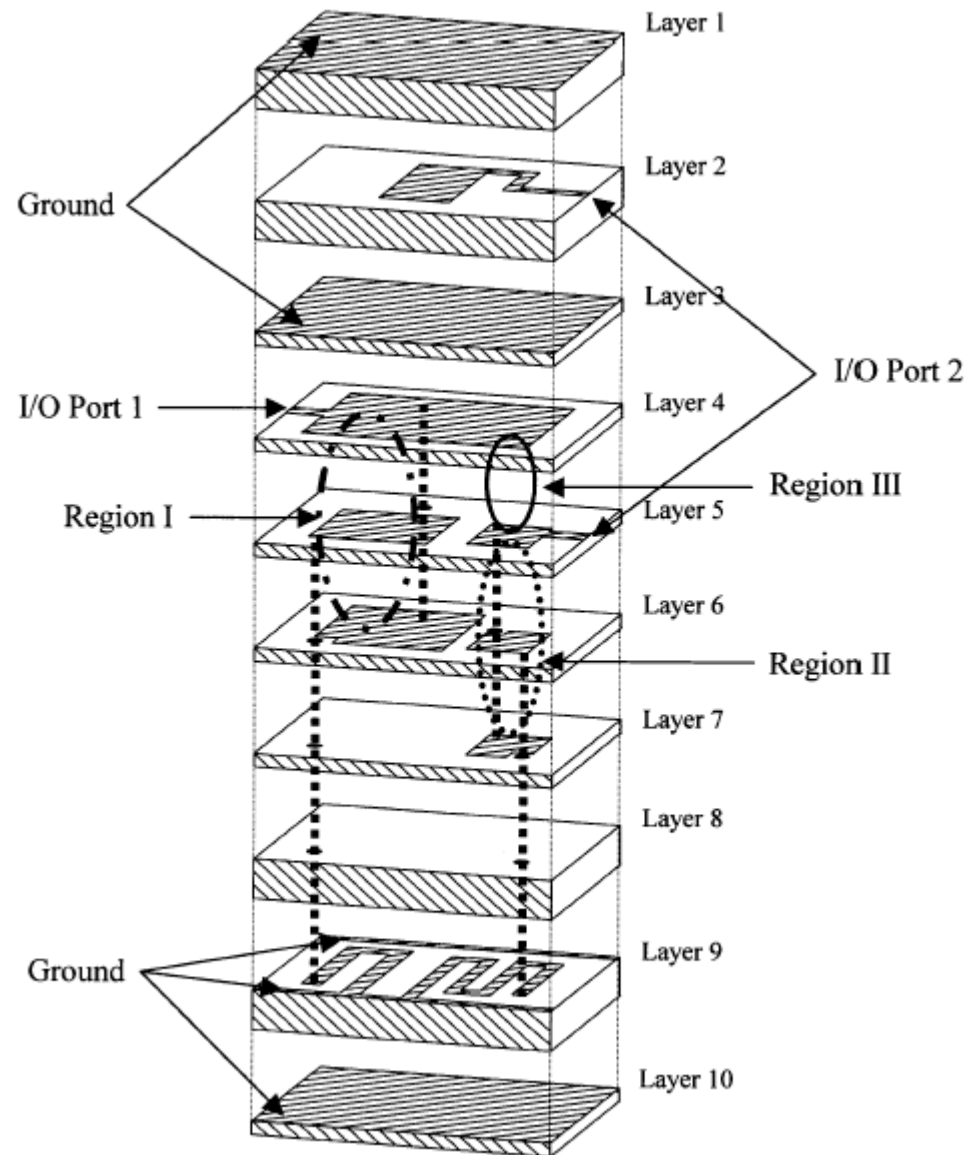
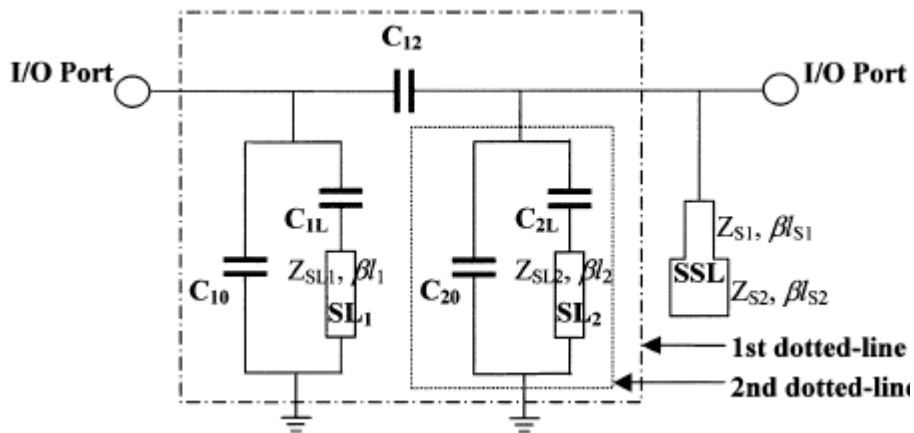
# Concept of multilayer filter (1/2)



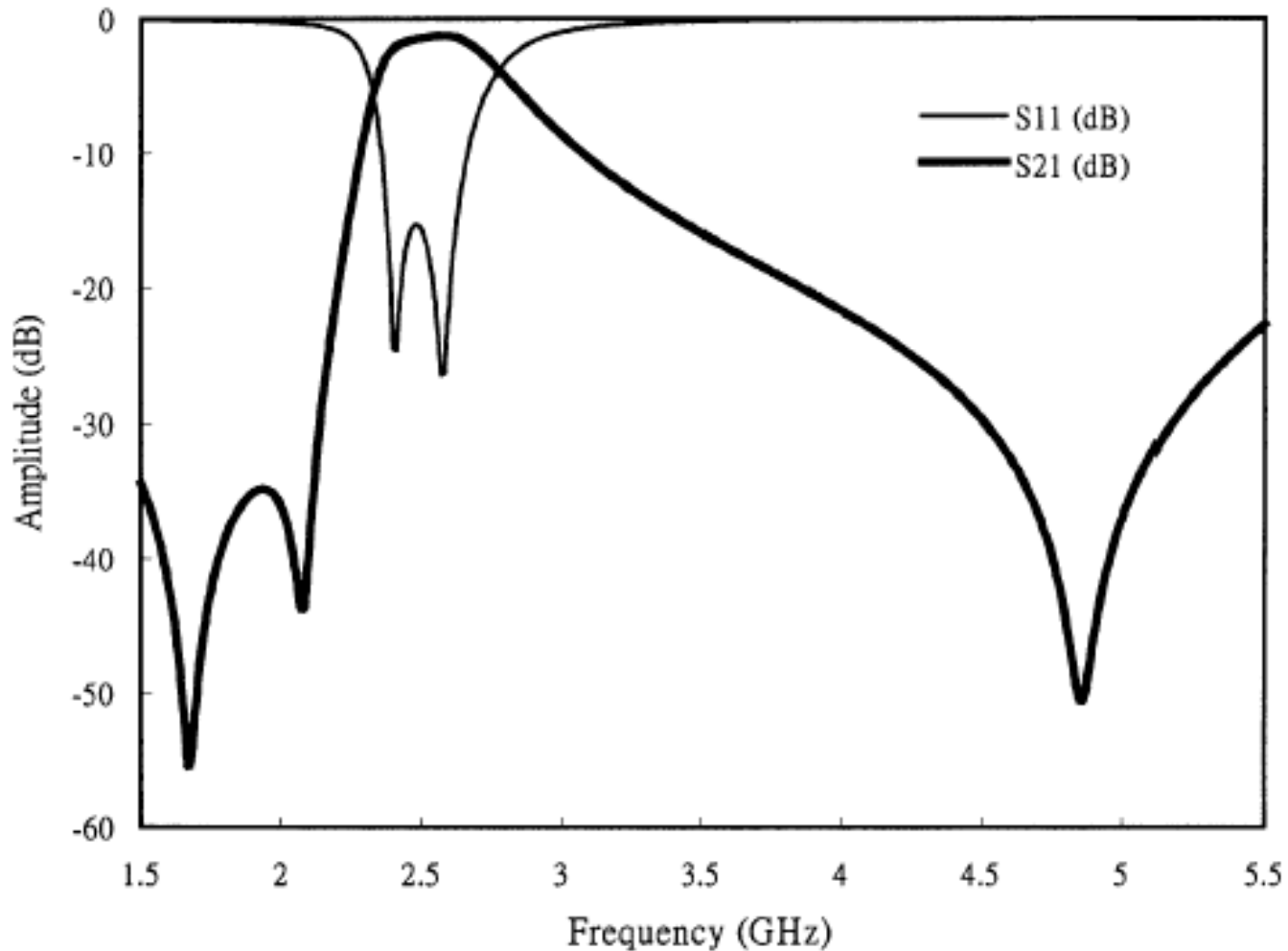
# Concept of multilayer filter (2/2)



# LTCC structure

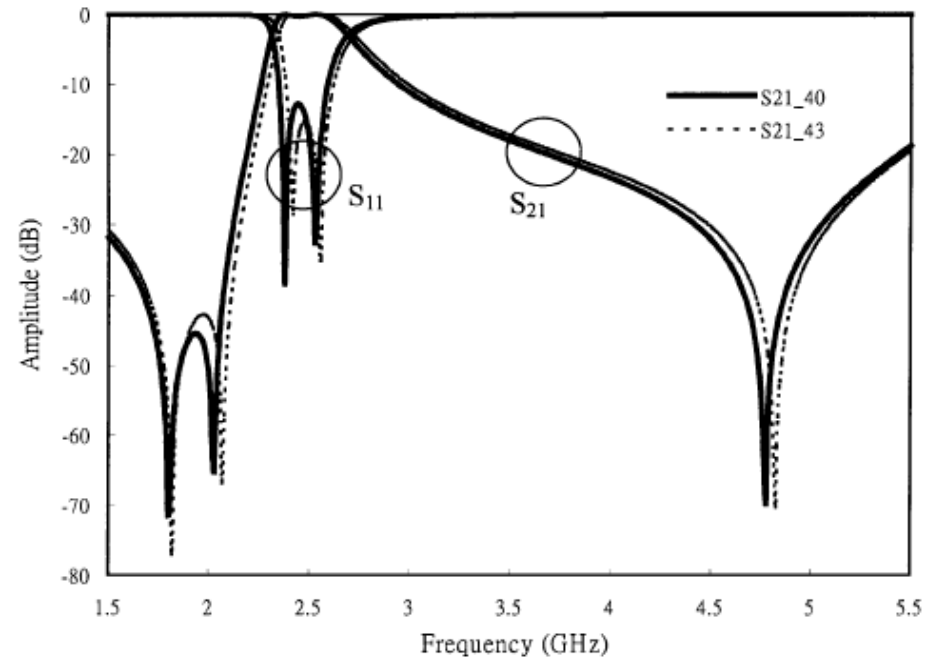
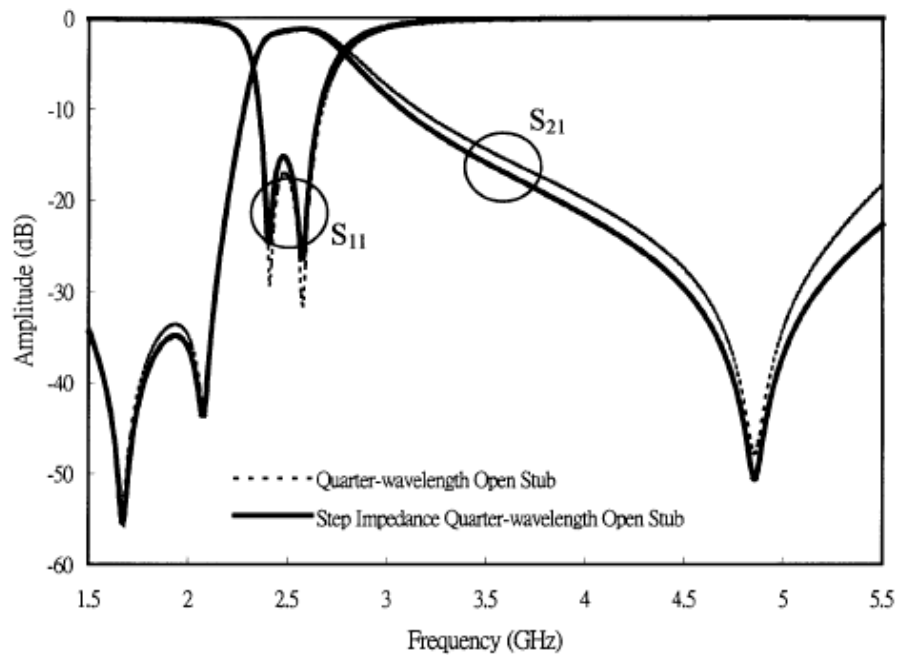


# Simulated result of the LTCC BPF

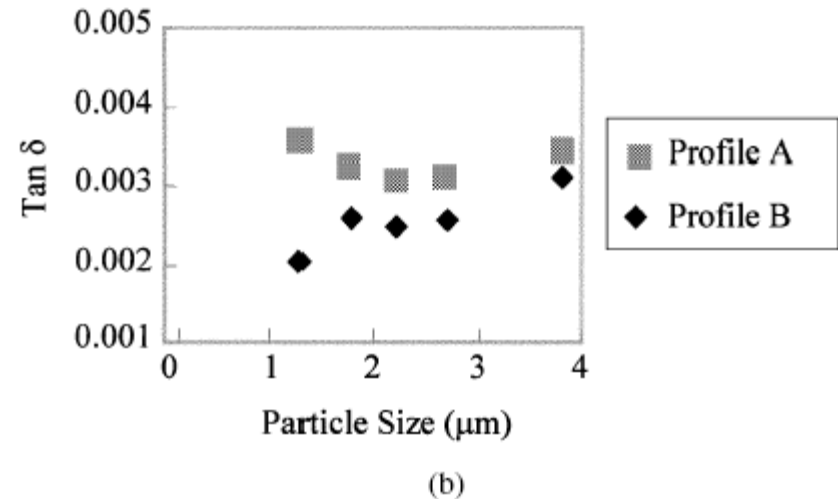
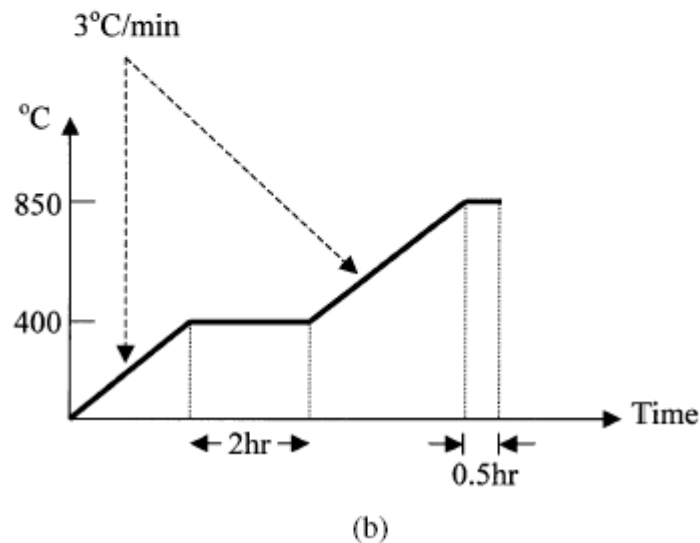
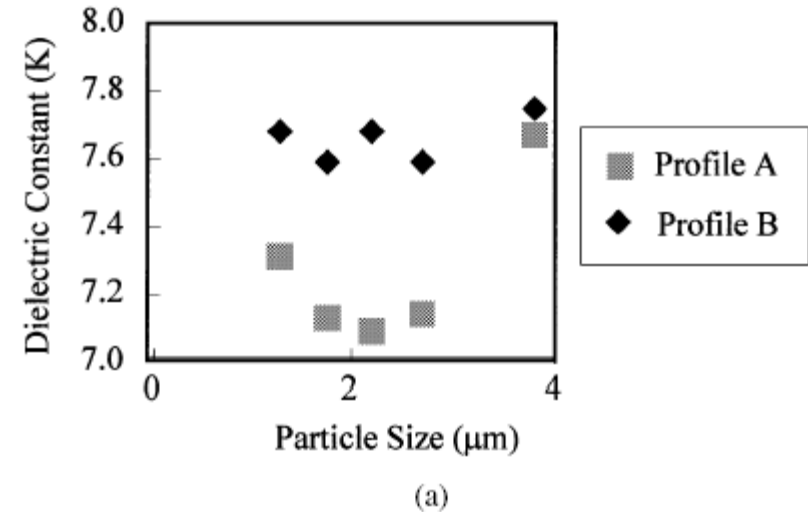
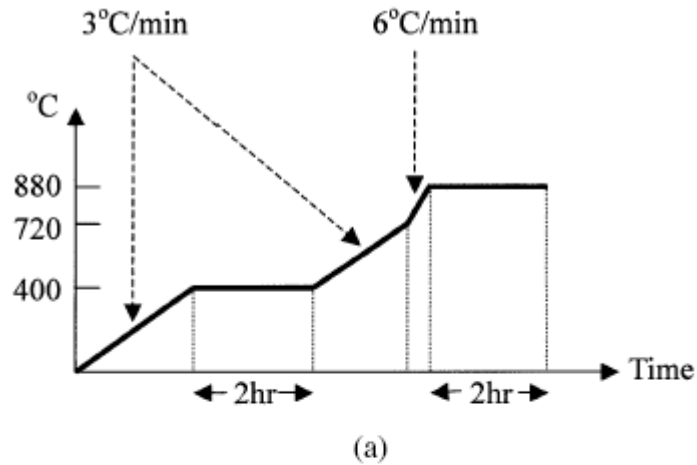




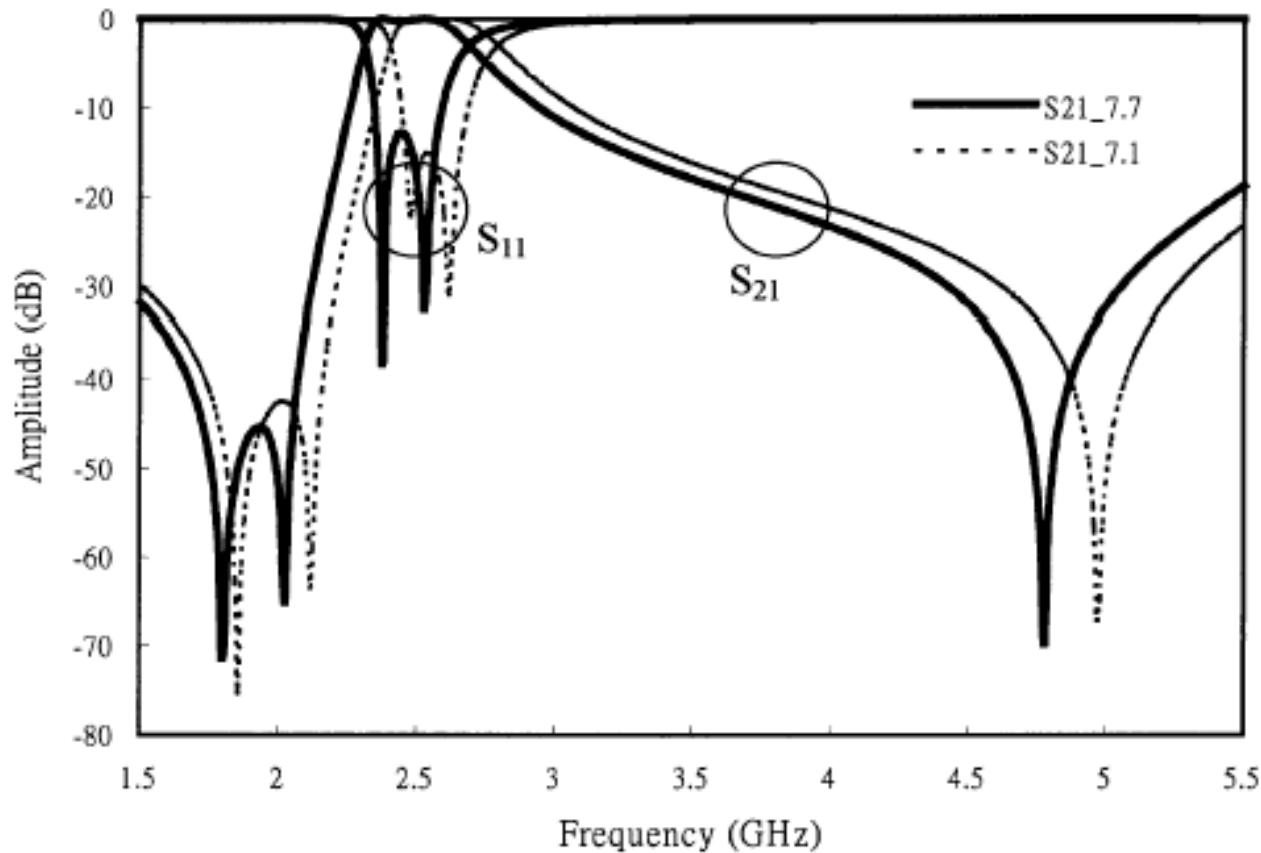
# Differences of stub and layer thicknesses



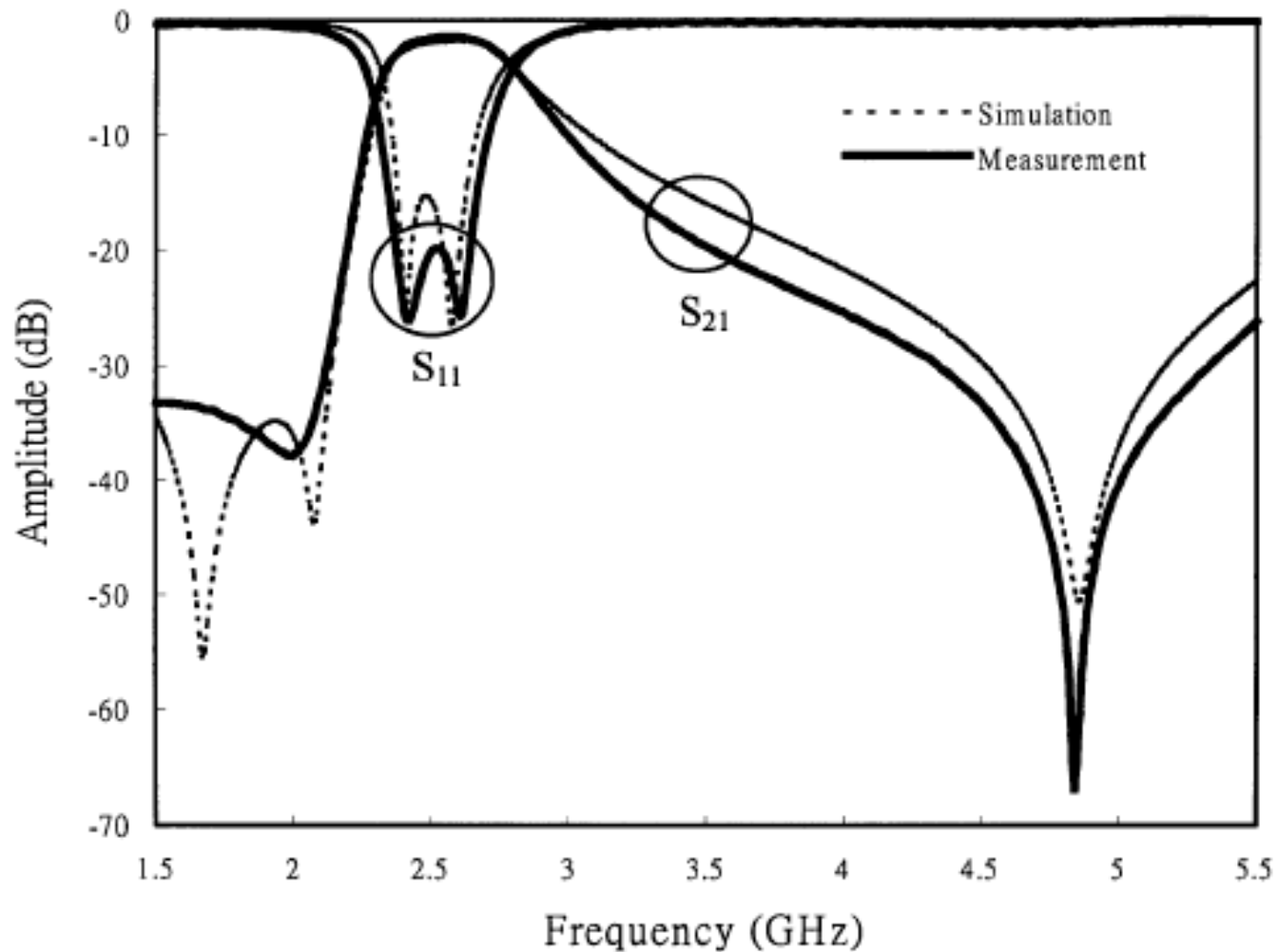
# Two different sintering profiles



# Simulated with two different dielectric constants



# Measurement





# Outline

- **What is LTCC?**
- **Advantages**
- **Process of LTCC**
- **Applications of LTCC**
- **Future developments**
- **Case study**
- **Conclusion**



# Conclusion

- Size and weight reduction is the trend of wireless or mobile communication, and LTCC seems to be the most efficient method.
- Zero shrink variation is the important future work of LTCC.

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